

Scientific Drilling

DRILLING MOTOR HANDBOOK

THE ULTIMATE PARTNER IN WELLBORE PLACEMENT

Scientific Drilling International (SDI) is an independent service provider offering a complete high accuracy wellbore placement and drilling solution. We are globally positioned to support a wide range of markets including Oil & Gas, CBM/CSG, Geothermal, and Mining Industries.

We are committed to make it easy for our customers to do business, by providing exemplary service and innovative technology. We earn loyalty one job at a time. We match the right crew to each assignment, and we hold ourselves accountable to the highest standard of quality.

We provide a full suite of drilling technology and services:

- Directional Drilling
- Rotary Steerable Services

Well Planning

- MWD/LWD Services
- Magnetic Ranging
- Drilling Motor Services
- Wellbore Surveying
- Survey ManagementDrilling Engineering
- Cased Hole Services

PREFACE

This handbook is to be used as a guideline, as it contains general information about SDI's drilling motors and industry accepted operational procedures only, and not suited for every drilling environment. It is intended to familiarize the end user about working principles of SDI's drilling motors and their specifications.

SDI is committed to continuous improvements of the drilling motors and procedures.

To view the most recent version visit: www.scientificdrilling.com/motorhandbook.

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02 MOTOR DESCRIPTION

This section of the handbook is designed to provide the drillers and operators with a general description of SDI's drilling motors. Different motor configurations have varying performance characteristics, but share the same major components:

- Top Sub
- Rotor Catch Mandrel
- Bent (Transmission) Housing
- Power Section Flexible Transmission
- Bearing Pack Assembly
- Bit Box
 - Near-Bit Stabilizers

FIGURE 1. MOTOR COMPONENTS



TOP SUB

The top sub is utilized to house the rotor catch and bored for a float. If a dump sub is present, it is primarily used to prevent tripping out with a wet drill string and can be used in place of the top sub for an additional charge.

ROTOR CATCH SYSTEM

The rotor catch system consists of components that are installed into the top portion of the motor. The function of the catch system is to minimize the possibility of losing motor components in the hole if a catastrophic failure occurs.

An external motor connection failure causes a substantial pressure loss while on-bottom. In the event of a parted motor, the Bottom Hole Assembly (BHA) is picked up off-bottom and the catch system will activate. It will hold the separated motor together and cause a pressure spike to indicate to drilling personnel that the motor may be damaged. The motor should be tripped out immediately without over-pull or string rotation to improve the chances of successfully tripping out the entire motor.

POWER SECTION

The power section components include the rotor and the stator, which converts hydraulic energy of the drilling fluid into rotational horsepower as the fluid is pumped from surface.

The rotor is a long spiral shaft designed to fit inside a corresponding stator. It is manufactured from a solid bar of stainless steel and plated with hard industrial chrome or carbide coating. The coating protects the parent metal against corrosion and reduces the friction between the rotor and the stator.

The stator is the non-rotating member of the power section. It is made out of a seamless, heat-treated tube with an elastomer lining. The internal cavity of the liner has a spiral geometry designed to accept a rotor of compatible geometry and size. In a positive displacement power section, the rotor always has one less lobe than the stator. SDI offers specially designed elastomers to improve downhole performance.

When the rotor is inserted inside the stator, a certain number of cavities are formed along the length of the power section. The interference between the rotor and the stator lining seals these cavities. During the drilling operation, high pressure drilling fluid is forced through the cavities, causing the rotor to turn inside the stator. The geometrical characteristics of the rotor and the stator offset their longitudinal axes. In other words, the rotor has an eccentric motion inside the stator.

Power sections are categorized by size, rotor/stator lobe ratios, and the number of stages. Figure 2 (below) shows the cross-sectional view of the rotor and the stator profile with different lobe ratios.



FIGURE 2. ROTOR AND STATOR PROFILE

The following guidelines are suggested when selecting and operating any SDI motor:

- The rotational speed of the rotor is proportional to the rate of fluid flow through the power section
- The generated torque is proportional to the differential pressure across the power section
- Power sections with a higher lobe ratio generate more torque and have slower rotary speed than the ones with a lower lobe ratio. For example, a

95%" motor with a 5/6 lobe ratio will rotate the drill bit at a higher RPM and will have less output torque per stage than a 95%" motor with a 7/8 lobe ratio

 An increase in the stage length will proportionally increase the output torque capability with a resultant slower RPM at the same flow rate

FLEXIBLE TRANSMISSION

The flexible transmission is the link between the rotor and the bearing mandrel, which converts the eccentric motion of the rotor into the smooth concentric rotary motion of the bearing mandrel. It also transmits the torque and rotary motion, generated by the power section, to the drive shaft. The hydraulic down thrust of the rotor is also transferred to the bearing section through this component.

SDI's flexible transmission is manufactured from a high grade of heat-treated alloy. The rugged design of this critical component may incorporate a seal, dependent on lower end configuration.

BENT (TRANSMISSION) HOUSING

This component of the motor houses the flexible transmission coupling and connects the stator housing to the bearing housing. A specific bend amount, ranging from zero to three degrees $(0^{\circ}-3^{\circ})$, is machined into this housing to make the motor assembly steerable.

The bent housing is manufactured using a premium grade of alloy steel. Its contact surface with the formation is hard-faced to minimize wear during the drilling operation.

An adjustable bent housing may be used in place of the fixed bent housing. The adjustable bent housing allows

the operator to change the bend of the motor from zero to three degrees $(0^{\circ}-3^{\circ})$ on location.

BEARING ASSEMBLY

The main components of the bearing assembly consist of the bearing mandrel, standard roller thrust bearings and PDC thrust bearings, radial bearings, and flow diverter.

The bearing mandrel is a shaft designed to transmit the power and channel the drilling fluid to the drill bit. It is manufactured from a high grade of alloy and is heattreated for strength and toughness.

The thrust bearings are designed to sustain the weight on bit and bearing the downward hydraulic thrust load of the rotor.

The unique design of SDI's combination of PDC and standard roller thrust bearings enable the same set of bearings to carry the on-bottom as well as the off-bottom load. This important feature reduces the number of bearing races within the limited available space, reducing the bit to bend, and increasing the thrust load capacity and the life of the bearing pack.

The radial bearings rigidly support the bearing mandrel inside the bearing housing. They are designed to accept the radial forces generated during drilling, while keeping the bearing mandrel aligned and concentric with the axis of the bearing housing.

BIT BOX

The bit box is an integral part of the bearing mandrel. The outside diameter is sized to accept a specified box connection. While all external components of the motor are stationary relative to the drill string, the bit box is the only external component that has a rotary motion independent of the rotational speed of the drill string.

NEAR BIT STABILIZER

SDI motors are available with removable or integral stabilizers. The removable stabilizers are screwed on the bearing housing at our service facilities and configured to their specified torque values.

In the case clients wish to have the option of installing stabilizers on the motor at the rig site, the motor is shipped with a thread protector installed on the external threads of the bearing housing.

03 JOB PLANNING

When planning the job, it is essential to consider several factors in order to select the right motor for your specific application.

HOLE SIZE

The SDI drilling motor fleet was designed to support a wide range of hole sizes. The recommended hole size for each motor can be found in the Appendix section. We encourage consulting SDI personnel as any deviation could result in hole problems and/or cause premature motor failure.

REQUIRED DOGLEG SEVERITY

Refer to the Appendix for the predicted build rate for each size motor. The values listed in the Appendix should be used as a guideline only, since factors such as the bit type, formation characteristics, BHA configuration, Weight-On-Bit (WOB), rotary RPM, hole OD, etc., affect the actual build rate.

If the motor is intended for rotary drilling, refer to rotation limit plots in the Motor Specification section.

BIT SELECTION

The proper selection of the drill bit can substantially increase the penetration rate, reduce drilling cost, and improve motor performance.

The bit's Total Flow Area (TFA) affects both motor performance and the ability to clean the hole. An undersized bit TFA will result in high-pressure drop across the bit and lower than expected flow rate. Inadequate flow rate can result in overheating and damage to the bit, hole-cleaning problems, and will starve the motor of the adequate fluid needed to operate at its optimum performance. On the other hand, an oversized TFA might not provide the fluid momentum necessary to remove the cuttings properly. The formulas required to calculate the bit TFA are provided in the Appendix. The Motor Specification section of this handbook lists the recommended bit pressure drop for each size motor. If the flow requirements needed for your specific application exceed the maximum allowable motor flow rate, a bored rotor can be provided to supply the additional fluid for some power sections.

For angle building runs, the design of the bit's gauge and length becomes critical. High drag, Polycrystalline Diamond Compact (PDC) bits exert more stress on the motor components than traditional cone or less aggressive bits. Also, high RPM motors combined with high WOB require more flow to cool the bit. Contact the bit manufacturer for the minimum recommended bit flow rate and speed.

DRILLING FLUID

The most fluid-sensitive component of the SDI motor is its stator elastomer. Therefore, it is important that the type of mud and all of its characteristics are given to the SDI representative during pre-job planning. SDI's drilling motor fleet was designed to operate successfully with water-based mud, fresh water, brine, seawater, synthetic and oil-based mud. When drilling with an oil-based mud, the aniline point of the mud must exceed the downhole static temperature to maximize the stator lining life. The mud manufacturer will be able to provide the aniline point of the mud.

The pH level of the drilling fluid can affect the life of the drilling motor. The recommended pH level is between 4 and 10 for SDI motors.

If there is a prolonged interruption in drilling, periodic circulation through the motor will increase motor life, as the stagnation of fluid inside the motor will cause deterioration.

The solid content of the drilling fluid should be maintained below 5% and the sand content below 2%. Any deviation from the specified limits will cause the bearings and elastomer lining to wear rapidly, which will result in a gradual reduction in the output power of the motor.

Mud weight is another factor that should be considered when planning the drilling operation. Generally heavier mud (12 lb/gal [14.37 kg/m3] or greater) will wear the motor at a faster rate than lighter mud. When using heavy drilling fluid, keep the sand content below 0.5% to minimize a possible washing in the drilling motor.

Any additives to the mud system should be carefully selected to comply with these specifications.

If a substantial amount of gas or air is trapped in the drilling fluid, it should be removed to prevent any possible damage to the stator rubber.

Medium to fine lost-circulation material can be used, as long as they are mixed thoroughly. If the drilling conditions require the use of coarse material, we recommend the use of jet subs above the motor to bypass a portion of the particles and prevent plugging.

The use of solid additives with rough or sharp texture should be avoided, as they have the potential to scar or cut the stator rubber lining.

HOLE TEMPERATURE

Bottom hole static temperature affects the physical and mechanical properties of the stator's elastomer. Therefore, it is important that the expected temperature range is given to the SDI representative during pre-job planning. An increase in temperature decreases the mechanical strength of the stator's rubber lining and may cause temperature related swelling. Excessive interference increases the frictional heat generation and will over-stress the rubber compound, resulting in premature stator failure.

SDI calculates the rotor/stator interference to provide the needed power in all sections of the well based on average expected downhole temperature. Figure 3 illustrates the reduction in the tensile strength of the stator elastomer lining as the temperature increases.

Any reduction in the differential pressure of the motor while drilling will significantly increase the life of the elastomer.



POWER SECTION RATED PERFORMANCE

Figure 3. Temperature effects on Tensile strength

To increase the motor life, certain cautionary measures should be employed when drilling in a hot-hole environment. These measures are addressed in the Motor Operation section of the handbook.

ROTOR NOZZLE USAGE

With the exception of high-speed power sections (1:2 lobe ratio), most SDI rotors are bored to allow various size nozzles. Rotor nozzles are used to increase the flow rate at the bit by directing a portion of the fluid through the rotor. The use of a rotor nozzle is recommended when system hydraulics require a flow rate that exceeds

the maximum allowable flow through the motor. Refer to the Appendix for proper sizing of the nozzle.

POWER REQUIREMENTS

When selecting a motor, pay close attention to its maximum power output. The motor should be powerful enough to deliver the required amount of torque, at the right RPM, to turn the drill bit in response to the application of various WOB.

Most SDI motors are available with hard rubber in all power sections, which can increase the Rate of Penetration (ROP), decrease stalling, and drill harsh formations with more ease than a standard motor power section.

AIR DRILLING

When drilling a well using air or foam, special consideration must be taken when selecting the power section. SDI's air motors are provided in a high torque, low speed power section minimize the severity of off-bottom runaway speed that may be encountered in air drilling operations. Refer to SDI's product specification sheets for more details.

SDI recommends a non-petroleum based lubricant to be injected into the dry air at surface in order to provide lubrication to the moving parts inside the motor. On dry air, this is a best practice to keep the stator cool. The lubricant should be at least 3% soap concentration.

SDI recommends high accuracy pressure gauges that indicate 25 psi (172 kPa) increments to be fitted to surface lines. When making connections, the pressure should be allowed to bleed off, and reduce the flow rate by half when starting a motor after connections.

04 MOTOR OPERATION

This section provides a general guideline regarding the use of SDI drilling motors.

SDI's drilling motors arrive at the rig site with all internal and external connections made-up to the specified torque. The near bit stabilizer, if requested, is installed and made-up to the full recommended torque value. The bit box and top sub connections, selected by the customer, are then fitted with thread protectors. Once the drill bit is installed, the motor is ready for operation.

SURFACE TESTING

Testing tools on surface prior to use is recommended to minimize the risk of operational issues once the tool is downhole. Surface motor tests should be conducted without the bit in order to avoid potential damage.

Recommended testing procedures:

- Use correct lift sub at all times. Also, ensure lift sub and drilling motor connection is sound by testing with a chain tong. Lift motor with top drive or elevators and set in slips. Safety clamps and dog collars are recommended.
- Connect the motor (to top drive or kelly) after removing the lift sub. Remove the dog collar/safety clamp, then raise the motor out of the slips.
- 3. The motor should be lowered until the bit box is just below the rotary table, with the bit box still in sight.
- 4. Gradually begin pumping, increase the flow rate until the bit box is turning.
- 5. There should be some leakage noted coming from above the bit box.
- 6. Gradually increase the flow rate to the minimum according to the motor specifications and record flow rate and pressure.

7. Turn flow off and check thrust bearing clearance by performing a squat thrust test. Reference Table 2 (below) for acceptable wear specifications.

Table 2

Allowable Thrust Bearing, Radial Bearing, and Coupling Wear of the Bit Box

| Motor Size | Maximum Axial Play | | Maximum Circumferential Play | | Maximum Radial Play | | | |
|---------------|-----------------------|---------|------------------------------------|-----|------------------------|---------|--|--|
| | TiTAN22 | | | | | | | |
| 5.00" | 0.100" | 2.54 mm | N/A | N.A | 0.043" | 1.09 mm | | |
| 5.15" | 0.100" | 2.54 mm | N/A | N/A | 0.052" | 1.32 mm | | |
| 6.60" | 0.100" | 2.54 mm | N/A | N/A | 0.052" | 1.32 mm | | |
| 7.15″ | 0.100" | 2.54 mm | N/A | N/A | 0.065" | 1.65 mm | | |
| 9.15" | 0.130" | 2.54 mm | N/A | N/A | 0.065" | 1.65 mm | | |

INSPECTIONS BETWEEN RUNS

- Evaluate all stabilizers for wear and damage prior to attempting another run
- Turn flow off and check thrust bearing clearance by performing a squat thrust test. Reference table 2 for acceptable wear specifications
- Drain all drilling fluid from tool by rotating bit box clockwise
- Flush the tool with fresh water or non-petroleum oil if the tool will be laid down

TRIP IN GUIDELINES

- Minimize the amount of stationary assembly time
- Descend at a controlled rate
- Trip the drill string with the blocks unlocked
- Use caution when approaching BOP, liner hanger, casing shoe, bridges, known tight spots, ledges or bottom

- Slowly ream through tight spots with maximum recommended flow rate and string rotation of 30 RPM or less
- Circulate occasionally to both avoid plugging the nozzles of the bit and when temperatures are above 250°F (121°C) to cool the BHA
- PDC bits should not be circulated for extended periods of time without WOB to avoid bit damage
- If the float valve is not used and the drill string is empty, the annulus pressure combined with the dynamic pressure, generated while tripping in will force the drilling fluid through the bit and into the motor causing the motor to rotate in reverse. This could result in unscrewing or breaking one or more internal components. It is recommended to use at least one float, and if not feasible, keep the drill string full at all times and trip in slowly. SDI recommends filling the pipe every 500 ft
- Approximately 100 ft from bottom, start pumps and trip in at a controlled speed ensuring not to spud the motor

STAGING

Motor preparation procedures for High Temperature operations

- Normal tripping in procedures should be practiced until arriving at a depth with a predicted temperature of 250°F (121°C) or greater.
- 2. Once the measured depth with the predicted temperature is reached, break circulation to cool the BHA
- 3. Circulate for approximately 5 min at every fill point
- 4. Once drilling operations have begun, gradually apply differential pressure to the recommended maximum reduced differential pressure
- 5. Refer to Power Section Rate of Performance chart

High Temperature Guidelines

High temperature wells are defined as wells with a downhole temperature above 250°F (121°C).

Motor Preparation Procedures in Cold Temperature Operations

- 1. It is critical to warm a motor prior to operations in cold temperatures.
- 2. Heat the entire motor, from the bit box end, using steam until it is warm to the touch.
- 3. Do not heat the motor rapidly or inconsistently to prevent internal component damage. A general practice is to heat over a 60 min period.

HOLE OD RESTRICTIONS

Use caution when motor with bent sub or non-zero angle housing travels through BOP, liner hanger, casing shoe, bridges, known tight spots, ledges or bottom

WASHING AND REAMING

Maintain flow rate above minimum requirements to clean and cool the motor bearings. It is recommended to flow as much as possible without exceeding maximum to easily identify stalls.

To avoid motor damage, limit reaming with minimal WOB, and maximum flow for which that power section has been rated.

While cleaning and backreaming, do not exceed the recommended speeds located on the rotational limit charts. Also, ensure you maintain flow rate and lower string rotation speed when working through a tight spot.

Do not backream with a motor under these circumstances:

• More than 90 ft (30 m) of backreaming

- Excessive tension on the motor while backreaming may cause damage to thrust bearings and mandrel wear
- It is not recommended to rotate the motor at greater RPM or through higher doglegs than what is specified on the rotational limit chart

DRILLING PROCEDURES

- Gradually increase flow rate to the desired GPM (LPM) once the bit is 6-10 ft (2-3 m) off-bottom, while not exceeding the maximum flow rate of the power section. If available, it is recommended to set the automatic drilling system to slowly tag bottom. Once the bit is 1-2 ft off-bottom ensure the WOB and differential pressure is zeroed.
- 2. Monitor flow rate and pump pressure (side loads may affect calculated off-bottom pressure)
- 3. Perform drill-off test to determine ideal differential pressure and WOB

SLIDING

Prior to orienting for a slide, gradually work out any drillstring torque. Orient the tool face with the consideration of the BHA reactive torque and lock the rotary table or top drive. Use caution to avoid stacking weight, which can potentially release, causing damage to the motor and loss of tool face control.

ROTARY DRILLING

All motors can be used for rotary drilling operations, with the maximum possible string RPM dependent on the bend angle.

High drillstring RPM will cause excessive bit speeds and excessive wear to the BHA. Stick slip effects can cause instantaneous BHA rotation speeds up to three times the surface RPM resulting in severe damage to downhole tools. Higher rotary speeds may be necessary in some circumstances, but the life expectancy of the motor and other downhole equipment will be reduced.

ROTARY RPM

While rotating, a lateral force is exerted on the drill bit by the formation. The magnitude of the force is directly proportional to the bit to bend length, bend angle, dog leg severity, and formation hardness. The induced bending stress on the motor increases the risk of fatique failure. Reference rotational limit charts for string rotation speeds.

Note: When transitioning from sliding to rotating, pull back until the bit is above the slid interval. Then, using a maximum rotary RPM of 25, carefully ream back to bottom. Maintain this low RPM until the bit to bend length is drilled off.

STALLING

A stall occurs when the rotor stops rotating while the drilling fluid continues to flow through the motor. During a stall, the stator elastomer is pushed aside resulting in severe stresses within the elastomer and eventually fatigue failure of the stator as well as high stresses of the transmission and bearing section, which can result in catastrophic damage.

A short occurrence of the power section not supplying the needed torque for the bit to continue rotating is defined as a microstall, which in multiples is just as damaging as a hard stall. High WOB and rotating in large dog legs increases the chances of microstalling.

Note: Stalling during rotary drilling (over running the bit) is not as noticeable as stalling while sliding. Stalling while rotating causes more damage to the stator elastomer due to the rotor rotating in reverse while drilling fluid continues to flow through the power section. If a stall is encountered on a Kelly drive:

- 1. Stop rotation immediately.
- 2. Reduce flow rate by at least 50%.
- 3. Use rotary table brake to gradually release stored torque.
- 4. Pick off bottom slowly.
- 5. Stage pumps back to normal operating flow rates and pressure. Monitor pressure and slowly resume drilling operations. If abnormal pressures continue, or unable to drill consult Onsite Drilling Manager and SDI personnel for confirmation to trip out. Refer to the rotor catch tripping instructions if excessive pressures are encountered.

If a stall is encountered on a Top drive:

- 1. Stop rotation immediately.
- 2. Reduce flow rate by at least 50%.
- Lock brake on the top drive, gently hoist to string weight, and slowly release the brake on the top drive to release the trapped torque. The lower string weight will greatly reduce the trapped torque, which will lessen the backlash/whip.
- 4. Pick bit off-bottom slowly.
- 5. Stage pumps back to normal operating flow rates and pressure. Monitor pressure and slowly resume drilling operations. If abnormal pressures continue, or unable to drill consult Onsite Drilling Manager and Directional Coordinator for confirmation to trip out. Refer to the rotor catch tripping instructions.

PRESSURE DROP

Do not exceed maximum recommended differential pressure or circulation rates, as this will reduce the life of the stator elastomer and bearing assembly. Refer to Motor Specification section for maximums.

INCIDENT ASSESSMENT ACTIONS

The following is a list of the most commonly observed motor difficulties:

Sudden Pressure Increase

- Stalled motor
- Bit or tool plugged
- Seized bearing assembly
- Suspected rotor catch engagement

Low/No Penetration

- Worn bit
- Formation change
- Stabilizer hang up
- Damaged or worn stator elastomer

Slow Pressure Decrease

- · Drill string or dump sub washout
- Lost circulation
- Well control issue

Sudden Pressure Decrease

- Back-off in the drill string or on the motor
- Fracture of the driveshaft assembly

Bit Box Does Not Spin While Circulating

- Backed-off connection
- Fracture of the driveshaft assembly
- Severe lost circulation

Bit Box Does Not Spin, Minimal Flow When Circulating

- Seized bearing assembly
- Chunked stator elastomer
- Partial plugging within the drillstring

VIBRATION

Vibration can cause the most significant motor fatigue and should be mitigated in order to avoid downhole failures.

These are the 3 types of drilling vibration:

- Torsional Vibration (Stick Slip)
- Lateral Vibration
- Axial Vibration

Reference Shock and Vibration Limitations section in the Appendix for more information.

TORSIONAL VIBRATION

Torsional vibration can be attributed to alternating speeding up and slowing down of the BHA while rotating, as the bit/formation interaction may cause the bit to stop momentarily. When the bit instantaneously stops, the drill string continues turning with increased torque, which then frees the bit to accelerate (otherwise known as bit whirl). BHA induced stick slip, which occurs when contact points become stuck, can have a similar effect. This can cause connections to back off or damage to all BHA components.

Symptoms

- Large and erratic surface RPM and torque fluctuations, especially noticeable on a top drive
- Fluctuating sound from top drive or kelly
- Cutter/insert damage; bit/stabilizers wearing under-gauge
- Poor hole cleaning, under-gauge or washed out hole
- Shock/vibration measurements received from MWD
- Connection fatigue cracks; fractures of BHA components; connection back-off

- Fractured or cracked motor drive line components such as bearing mandrels or transmissions
- Erratic increase and decrease in surface torque.
- Top drive stalling
- Increase in lateral vibrations
- Housing or connection fracture
- Chipped cutters/excessive bit wear

Solutions

- Improve the lubrication qualities of the drilling fluid
- Adjust operating parameters (i.e. increase RPM or decrease WOB
- Pick up off-bottom and work out all drillstring torque
- Drill with less aggressive PDC bit
- Use alternative BHA components or placement

LATERAL VIBRATION (BIT/BHA WHIRL)

Lateral vibration occurs when the BHA comes into contact with the side of the wellbore. This causes drilling inefficiencies, as well as damage to BHA components.

Causes

- Harmonic resonance of drill string
- Excessive RPM and stick slip
- Low WOB with High RPM
- Lack of lubrication in mud
- Reaming/backreaming, hole opening, or drilling out of casing

Symptoms

- Poor penetration rates and higher Mechanical Specific Energy (MSE) than expected from that formation
- Damage to the bit is probably in the shoulder or randomly scattered across the body. Dull characteristics will be chipped and broken or missing cutters
- Rotary torque fluctuations

Solutions

- Pick up off-bottom and hold string stationary until all energy is released (typically a couple minutes)
- Increase WOB, reduce RPM and try to confirm with downhole measurements while drilling
- Improve the lubrication qualities of the drilling fluid

DETECTING LATERAL VIBRATIONS

- Erratic fluctuations in surface torque created by severe stick slip usually accompanies high lateral shocks
- Slower ROP

MITIGATING LATERAL VIBRATIONS

- Pick up off-bottom to work out all torque and vibration
- Change RPM or change WOB
- Modify BHA (i.e., add stabilizer)

AXIAL VIBRATION

Axial vibration, also known as "bit bounce," is caused by a cyclical loading and unloading of the bit and the BHA in the axial direction. It is characterized by rapid cyclical movement of the neutral point in the BHA that causes the WOB to quickly increase and decrease.

Causes

- Excessive RPM
- Excessive WOB with high RPM
- Erratic fluctuations of the WOB/hook load
- Visible bouncing motion of the top drive and kelly hose
- Slower Rate of Penetration (ROP)
- Excessive damage/wear to bit

Symptoms

- Large WOB fluctuations (shaking hoisting equipment)
- Damage to the bit, broken cutters on cones, particularly the outer rows
- Internal inspection of bearings may find excessive wear
- High downhole vibration as recorded by MWD/LWD tool

Solutions

- Change RPM and WOB combinations to get a stable drilling situation and the MWD axial sensor will inform the directional driller that the vibration has been eliminated
- Pick up off-bottom/work out all torque
- Decrease RPM or WOB

ROTOR CATCH FUNCTIONING

The rotor catch is designed to mitigate losing a portion of the motor in the event of a housing connection failure.

If a connection back-off occurs, it must be identified quickly. Features for identification:

- Pressure loss when the bit is on-bottom (due to loss of flow through housing)
- When the motor is off-bottom the standpipe pressure will increase

- With WOB reapplied, the pressure increase disappears
- BHA should not be rotated if possible
- Circulation should be kept to a minimum
- SDI's directional personnel should be present during trip out

TRIP OUT PROCEDURE

Drilling fluid will typically drain from the lower end of the bearing assembly while the motor is tripping out of hole. When tripping through high-angle curves, ensure tool face is highside. Avoid rotating drill string, which can cause damage and wear to the bit and motor.

LAY-DOWN PROCEDURES

SURFACE CHECKS BEFORE LAY-DOWN

- 1. Surface check inspection procedures should be repeated with attention paid to the functionality; bit box rotation, fluid bypass rate above the bit box, and axial and radial movement of the bottom end of the drilling motor.
- 2. A mud lubricated drilling motor lay-down review should be performed if the drilling motor is going to be rerun.
- 3. Review takes into account extreme drilling conditions and allows reuse of drilling motor based on mandatory limits, in combination with the operator's judgement.
- 4. Drain the motor by rotating the bit box.

GENERAL PRACTICE

It is important to flush the drilling motor with fresh water or non-hydrocarbon oil before laying it down. Failure to do so will allow the drilling fluid to further deteriorate components long after the drilling motor has been operated.

05 MOTOR SPECIFICATIONS

This section of the handbook provides critical information regarding the physical characteristics and performance parameters of SDI's drilling motors. They are classified as Standard, Performance and Air motors.

SDI is committed to ongoing improvements of drilling motors and procedures. As a result, the information in this handbook is subject to change without notice.

The flow rate, RPM, torque, and differential pressure correlation is presented graphically for each motor. The proper interpretation of these graphs is crucial in maintaining the specified operating limits of the motor.

HOW TO INTERPRET THE GRAPHS

Figure 1 on page 32 shows a typical graph used to determine the performance of a specific motor. Using this graph, the RPM and the output torque of the motor can be determined at a certain differential pressure.

To determine the approximate motor RPM, follow this procedure:

- 1. Locate the desired differential pressure on the corresponding axis.
- From this point, draw a vertical line until it intersects the RPM curve at the desired gal/min (L/min).
- From the point of intersection, draw a line perpendicular to the RPM axis to find the corresponding bit rotary speed. For example: a 6¹/₂" SDI motor with a 7/8 lobe ratio and 5.0 stages operating at 400 psi (2,758 kPa) of differential pressure and 600 gal/min (2,271 L/min) is about 174 RPM.
- 4. The RPM graph can be extrapolated to reflect the flow rates not shown on the graph. For instance,

to determine the RPM of the motor at 525 gal/min (1.987 L/min), draw a curve, parallel to the other curves, in the mid-point between the 600 gal/min (2,271 L/min) and 450 gal/min (1,703 L/min). Use this curve to determine the motor RPM at 525 gal/min (1,987 L/min) and a certain differential pressure.

To determine the output torque of a certain motor, follow these steps:

- 1. Locate the desired differential pressure on the corresponding axis and draw a perpendicular line until it intersects the torque line.
- From the point of intersection, draw a line perpendicular to the torque axis to find the corresponding output torque. For example, a 6¹/₂" SDI motor with a 7/8 lobe ratio and 5.0 stages operating at 400 psi (2,758 kPa) of differential pressure has an output torque of about 3,720 ft-lb (5,044 Nm).



Figure 1: Performance Graph

HOW TO USE ROTATION LIMIT PLOTS

- 1. Determine the wellbore curvature (DLS) that the motor is currently in.
- Draw a vertical line from the motor bend angle value on the x-axis upwards to the appropriate DLS curve (DLS, between curves provided, should be estimated by splitting the difference between two previously drawn curves).
- Draw a horizontal line from the point where the vertical line (step 2) intersects with the DLS curve, to the corresponding RPM value (y-axis) in that scenario.



EXAMPLES:

 Basic Chart Use - A 5°/100 ft curve has been drilled with a 1.75° Motor Bend. You would then, reasonably be able to rotate at 70 RPM within at that curvature. Once you've drilled away from the base of the curve, and the bend is now in a straight and enlarged hole, the effective DLS is now 0°/100 ft and the new allowable RPM is around 84 (Refer to red dashed lines in Figure 1).



2. Adding a DLS Curve - A hypothetical, 8 °/100 ft, curve is drilled entirely while sliding, with a 1.9° bend in the motor. First, a DLS curve for 8°/100ft must be drawn on the figure. Understanding that 7.5°/100 ft DLS curve would be in the middle between the 5°/100 ft dashed curve and the 10°/100 ft solid curve, an 8°/100 ft curve can be placed slightly to the left of where the 7.5°/100 ft curve would go (refer to red dashed curve in Figure 2). Once the DLS curve is determined, the same procedure that was used in Example 1 can be followed to determine the RPM limits.



Figure 2: Illustration of Example 2

3. "Out of Spec" Rotation - Ex: a 20°/100ft is drilled with a 2.3° motor bend. According to the chart, rotating once you've landed this curve would be "out of spec". In this scenario, a low RPM (maximum of 30) would have to be used until the bend is effectively out of the curve and in a straight wellbore. Once in a straight wellbore, RPMs can be increased to 50 (refer to red dashed line in Figure 3).



*Chart data is based on bending-moment limitations of the bent housing. The primary criteria used to establish these limit lines is the bending moment that results in the onset of shoulder separation at the bend. The plot is representative of a sustainable operation in a specific wellbore curvature (DLS). The chart only applies to slick motors and does not, in any way, attempt to predict build/ drop tendencies of the BHA. DLS lines correspond to the wellbore curvature that the motor is currently in. If a particular bend assembly is in a curve that, according to the chart, prevents rotation, then slowly rotate (30 RPM) until the motor has effectively drilled itself out of the curve. Prolonged rotation in a curve (>10 minutes) or sustained rotation rates above 30 RPM will accelerate fatigue in the motor and are considered out-of-spec operations. Configurations with stabilizers and special equipment need to be looked at on an individual basis.

MOTOR SPECIFICATIONS SUMMARY TABLE

| Motor Name | | | TÏTAN22 | | | | | |
|-----------------------|----------------|-----------|-----------|-----------|-----------|-----------|--|--|
| Motor Size | inch | 5.00 | 5.00 | 5.00 | 5.15 | 5.15 | | |
| (OD) | mm | 127 | 127 | 127 | 131 | 131 | | |
| Lobe | config | 7/8 | 7/8 | 7/8 | 6/7 | 6/7 | | |
| Stages | num | 3.1 | 3.8 | 5.0 | 6.6 | 8.0 | | |
| Lawath | ft | 30.9 | 27 | 27.9 | 36.1 | 32.8 | | |
| Length | m | 9.41 | 8.22 | 8.50 | 11.01 | 9.99 | | |
| Recommended | in | 6-61/4 | 6-61/4 | 6-61/4 | 6-61/4 | 6-61/4 | | |
| Hole Sizes | mm | 152-159 | 152-159 | 152-159 | 152-159 | 152-159 | | |
| Max Bend Angle | deg | 2.38° | 2.38° | 2.38° | 2.38° | 2.38° | | |
| Bit to Bend | in | 40.6 | 40.6 | 40.6 | 45 | 45 | | |
| Length | m | 1.03 | 1.03 | 1.03 | 1.14 | 1.14 | | |
| Bit Box Connection | API Reg Box | 31⁄2 | 31⁄2 | 3½ | 3½ | 31⁄2 | | |
| Мах | lbs | 30,000 | 30,000 | 30,000 | 30,000 | 30,000 | | |
| WOB | DaN | 13,345 | 13,345 | 13,345 | 13,345 | 13,345 | | |
| Max Overpull | lbs | 60,000 | 60,000 | 60,000 | 60,000 | 60,000 | | |
| for Rerun | DaN | 26,689 | 26,689 | 26,689 | 26,689 | 26,689 | | |
| Overpull to | lbs | 120,000 | 120,000 | 120,000 | 120,000 | 120,000 | | |
| Yield Motor | DaN | 53,379 | 53,379 | 53,379 | 53,379 | 53,379 | | |
| Max Bit | psi | 750 | 750 | 750 | 750 | 750 | | |
| Pressure Drop | kPa | 5,171 | 5,171 | 5,171 | 5,171 | 5,171 | | |
| Opt Bit | psi | 100-600 | 100-600 | 100-600 | 100-600 | 100-600 | | |
| Pressure Drop | kPa | 690-4,136 | 690-4,136 | 690-4,136 | 690-4,136 | 690-4,136 | | |
| LCM Capability | nut plug | 40 lb | | |
| Max Differential | psi | 700 | 900 | 1,180 | 1,560 | 1,880 | | |
| Pressure | kPa | 4,810 | 6,200 | 8,200 | 10,700 | 13,000 | | |
| Stall Differential | psi | 1,050 | 1,410 | 1,860 | 2,450 | 2,970 | | |
| Pressure | kPa | 7,210 | 9,700 | 12,800 | 16,900 | 20,500 | | |
| Torque at Max | ft-lbs | 5,460 | 4,130 | 4,670 | 8,550 | 6,110 | | |
| Diff Pressure | Nm | 7,402 | 5,600 | 6,400 | 11,592 | 8,300 | | |
| Stall | ft-lbs | 8,190 | 6,500 | 7,350 | 13,460 | 9,630 | | |
| Torque | Nm | 11,104 | 8,900 | 10,000 | 18,249 | 13,100 | | |
| Flow | gal/min | 150-275 | 100-250 | 150-300 | 200-425 | 150-330 | | |
| Range | L/min | 570-1,041 | 380-950 | 570-1,140 | 760-1,608 | 570-1,320 | | |
| Speed Range | RPM | 47-95 | 50-140 | 90-190 | 90-180 | 120-280 | | |
| Speed | rev/gal | 0.32 | 0.54 | 0.62 | 0.46 | 0.79 | | |
| Ratio | rev/L | 0.08 | 0.14 | 0.16 | 0.12 | 0.20 | | |
| Torque | ft-lb/psi | 7.83 | 4.62 | 3.97 | 5.51 | 3.25 | | |
| Slope | Nm/kPa | 1.54 | 0.91 | 0.78 | 1.08 | 0.64 | | |

MOTOR SPECIFICATIONS SUMMARY TABLE

| Motor Name | | | | TiTAN22 | | |
|--|----------------|-----------|-------------------------------------|-------------------------------------|-------------|-------------|
| Motor Size | inch | 5.15 | 6.60 | 6.60 | 6.60 | 6.60 |
| (OD) | mm | 131 | 168 | 168 | 168 | 168 |
| Lobe | config | 6/7 | 4/5 | 5/6 | 7/8 | 7/8 |
| Stages | num | 10.4 | 7.0 | 8.3 | 3.3 | 5.0 |
| Lanath | ft | 36.5 | 30.9 | 38.3 | 33.8 | 29.6 |
| Length | m | 11.14 | 9.41 | 11.67 | 10.3 | 9.02 |
| Recommended | in | 6-61/4 | 7 ⁷ /8-8 ³ /4 | 7 ⁷ /8-8 ³ /4 | 71/8-83/4 | 71/8-83/4 |
| Hole Sizes | mm | 152-159 | 200-222 | 200-222 | 200-222 | 200-222 |
| Max Bend Angle | deg | 2.38° | 2.38° | 2.38° | 2.38° | 2.38° |
| Bit to Bend | in | 45 | 49 | 49 | 49 | 49 |
| Length | m | 1.14 | 1.2 | 1.2 | 1.2 | 1.2 |
| Bit Box Connection | API Reg Box | 31/2 | 41⁄2 | 41⁄2 | 41/2 | 4½ |
| Max | lbs | 30,000 | 60,000 | 60,000 | 60,000 | 60,000 |
| WOB Max Overpull for Berup | DaN | 13,345 | 26,689 | 26,689 | 26,689 | 26,689 |
| Max Overpull for Rerun Overpull to Yield Motor | lbs | 60,000 | 105,000 | 105,000 | 105,000 | 105,000 |
| | DaN | 26,689 | 46,706 | 46,706 | 46,706 | 46,706 |
| Overpull to | lbs | 120,000 | 210,000 | 210,000 | 210,000 | 210,000 |
| Yield Motor | DaN | 53,379 | 93,413 | 93,413 | 93,413 | 93,413 |
| Max Bit | psi | 750 | 1,000 | 1,000 | 1,000 | 1,000 |
| Pressure Drop | kPa | 5,171 | 6,894 | 6,894 | 6,894 | 6,894 |
| Opt Bit | psi | 100-600 | 100-750 | 100-750 | 100-750 | 100-750 |
| Pressure Drop | kPa | 690-4,136 | 690-5,171 | 690-5,171 | 690-4,136 | 690-5,171 |
| LCM Capability | nut plug | 40 lb | 40 lb | 40 lb | 40 lb | 40 lb |
| Max Differential | psi | 2,340 | 1,580 | 1,960 | 780 | 1,180 |
| Max Bit Pressure Drop Opt Bit Pressure Drop LCM Capability Max Differential Pressure Stall Differential | kPa | 16,130 | 10,894 | 13,500 | 5.400 | 8,200 |
| Stall Differential | psi | 3,510 | 2,360 | 3,080 | 1,230 | 1,860 |
| Max WOB Max Overpull for Rerun Overpull to Yield Motor Max Bit Pressure Drop Dot Bit Pressure Drop LCM Capability Max Differential Pressure Stall Differential Pressure Torque at Max Diff Pressure Stall Torque | kPa | 24,200 | 16,272 | 21,200 | 8,500 | 12,800 |
| Torque at Max | ft-lbs | 8,610 | 9,090 | 13,030 | 13,150 | 10,650 |
| Diff Pressure | Nm | 11,673 | 12,324 | 17,700 | 17,900 | 14,500 |
| Stall | ft-lbs | 12,920 | 13,630 | 20,530 | 20,710 | 16,770 |
| Torque | Nm | 17,517 | 18,480 | 27,900 | 28,100 | 22,800 |
| Flow | gal/min | 225-425 | 300-600 | 350-750 | 300-600 | 300-650 |
| Range | L/min | 852-1,608 | 1,140-2,270 | 1,320-2,840 | 1,140-2,270 | 1,140-2,460 |
| Speed Range | RPM | 157-300 | 149-298 | 130-290 | 50-90 | 80-188 |
| Speed | rev/gal | 0.70 | 0.49 | 0.38 | 0.15 | 0.29 |
| Ratio | rev/L | 0.19 | 0.13 | 0.10 | 0.04 | 0.08 |
| Torque | ft-lb/psi | 3.68 | 5.77 | 6.68 | 16.95 | 9.06 |
| Slope | Nm/kPa | 0.72 | 1.13 | 1.31 | 3.33 | 1.78 |

MOTOR SPECIFICATIONS SUMMARY TABLE

| Motor Name | | | TiTAN22 | | | | | |
|-----------------------|----------------|-------------|-------------|-------------|-------------|-------------|--|--|
| Motor Size | inch | 6.60 | 7.15 | 7.15 | 7.15 | 7.15 | | |
| (OD) | mm | 168 | 181 | 181 | 181 | 181 | | |
| Lobe | config | 7/8 | 5/6 | 5/6 | 6/7 | 7/8 | | |
| Stages | num | 6.4 | 8.3 | 11.2 | 7.1 | 9.4 | | |
| | ft | 33.8 | 39.2 | 42.5 | 42.5 | 42.5 | | |
| Length | m | 10.3 | 11.94 | 12.95 | 12.95 | 12.95 | | |
| Recommended | in | 71/8-83/4 | 81/2-97/8 | 81/2-97/8 | 81/2-97/8 | 81/2-97/8 | | |
| Hole Sizes | mm | 200-222 | 216-251 | 216-251 | 216-251 | 216-251 | | |
| Max Bend Angle | deg | 2.38° | 2.12 | 2.12 | 2.12 | 2.12 | | |
| Bit to Bend | in | 49 | 57 | 57 | 57 | 57 | | |
| Length | m | 1.2 | 1.44 | 1.44 | 1.44 | 1.44 | | |
| Bit Box Connection | API Reg Box | 4½ | 41⁄2 | 4½ | 41⁄2 | 41⁄2 | | |
| Max | lbs | 60,000 | 60,000 | 60,000 | 60,000 | 60,000 | | |
| WOB | DaN | 26,689 | 26,689 | 26,689 | 26,689 | 26,689 | | |
| Max Overpull | lbs | 105,000 | 110,000 | 110,000 | 110,000 | 110,000 | | |
| for Rerun | DaN | 46,706 | 48,930 | 48,930 | 48,930 | 48,930 | | |
| Overpull to | lbs | 210,000 | 240,000 | 240,000 | 240,000 | 240,000 | | |
| Yield Motor | DaN | 93,413 | 106,757 | 106,757 | 106,757 | 106,757 | | |
| Max Bit | psi | 1,000 | 1,000 | 1,000 | 1,000 | 1,000 | | |
| Pressure Drop | kPa | 6,894 | 6,894 | 6,894 | 6,894 | 6,894 | | |
| Opt Bit | psi | 100-750 | 100-750 | 100-750 | 100-750 | 100-750 | | |
| Pressure Drop | kPa | 690-5,171 | 690-5,171 | 690-5,171 | 690-5,171 | 690-5,171 | | |
| LCM Capability | nut plug | 40 lb | | |
| Max Differential | psi | 1,510 | 1,960 | 2,520 | 1,670 | 2,120 | | |
| Pressure | kPa | 10,400 | 13,500 | 17,374 | 11,600 | 14,580 | | |
| Stall Differential | psi | 2,370 | 3,080 | 3,780 | 2,630 | 3,170 | | |
| Pressure | kPa | 16,400 | 21,200 | 26,062 | 18,200 | 21,870 | | |
| Torque at Max | ft-lbs | 13,630 | 13,030 | 16,420 | 18,230 | 18,680 | | |
| Diff Pressure | Nm | 18,500 | 17,700 | 22,260 | 24,800 | 25,330 | | |
| Stall | ft-lbs | 21,470 | 20,530 | 24,630 | 28,700 | 28,020 | | |
| Torque | Nm | 29,100 | 27,900 | 33,390 | 39,000 | 37,990 | | |
| Flow | gal/min | 300-650 | 350-750 | 450-750 | 500-750 | 500-750 | | |
| Range | L/min | 1,140-2,460 | 1,320-2,840 | 1,890-2,840 | 1,890-2,840 | 1,890-2,840 | | |
| Speed Range | RPM | 80-188 | 130-290 | 180-300 | 80-170 | 144-216 | | |
| Speed | rev/gal | 0.29 | 0.38 | 0.40 | 0.23 | 0.28 | | |
| Ratio | rev/L | 0.08 | 0.10 | 0.11 | 0.06 | 0.08 | | |
| Torque | ft-lb/psi | 9.06 | 6.68 | 6.51 | 10.92 | 8.33 | | |
| Slope | Nm/kPa | 1.78 | 1.31 | 1.28 | 2.15 | 1.73 | | |

MOTOR SPECIFICATIONS SUMMARY TABLE

| Motor Name | | | TiTA | N22 | |
|-----------------------|----------------|-------------|-------------|-------------|-------------|
| Motor Size | inch | 9.15 | 9.15 | 9.15 | 9.15 |
| (OD) | mm | 232.4 | 232.4 | 232.4 | 232.4 |
| Lobe | config | 7/8 | 7/8 | 7/8 | 7/8 |
| Stages | num | 4.0 | 5.7 | 5.9 | 7.0 |
| | ft | 32 | 38.34 | 44.4 | 44.4 |
| Length | m | 9.75 | 11.68 | 13.53 | 13.53 |
| Recommended | in | 121/4-26 | 121/4-26 | 121/4-26 | 121/4-26 |
| Hole Sizes | mm | 311-660 | 311-660 | 311-660 | 311-660 |
| Max Bend Angle | deg | 1.83° | 1.83° | 1.83° | 1.83° |
| Bit to Bend | in | 66 | 66 | 66 | 66 |
| Length | m | 1.67 | 1.67 | 1.67 | 1.67 |
| Bit Box Connection | API Reg Box | 65/8-75/8 | 65/8-75/8 | 65/8 - 75/8 | 65/8-75/8 |
| Мах | lbs | 120,000 | 120,000 | 120,000 | 120,000 |
| WOB | DaN | 53,378 | 53,378 | 53,378 | 53,378 |
| Max Overpull | lbs | 100,000 | 100,000 | 100,000 | 100,000 |
| for Rerun | DaN | 44,482 | 44,482 | 44,482 | 44,482 |
| Overpull to | lbs | 250,000 | 250,000 | 250,000 | 250,000 |
| Yield Motor | DaN | 111,205 | 111,205 | 111,205 | 111,205 |
| Max Bit | psi | 1,000 | 1,000 | 1,000 | 1,000 |
| Pressure Drop | kPa | 6,894 | 6,894 | 6,894 | 6,894 |
| Opt Bit | psi | 250-990 | 250-990 | 250-990 | 250-990 |
| Pressure Drop | kPa | 1,723-6,205 | 1,723-6,205 | 1,723-6,205 | 1,723-6,205 |
| LCM Capability | nut plug | 40 lb | 40 lb | 40 lb | 40 lb |
| Max Differential | psi | 940 | 1,340 | 1,390 | 1,650 |
| Pressure | kPa | 6,500 | 9,300 | 9,600 | 11,376 |
| Stall Differential | psi | 1,490 | 2,110 | 2,190 | 2,600 |
| Pressure | kPa | 10,200 | 14,600 | 15,100 | 17,926 |
| Torque at Max | ft-lbs | 14,830 | 25,920 | 21,870 | 25,210 |
| Diff Pressure | Nm | 20,100 | 35,200 | 29,700 | 34,180 |
| Stall | ft-lbs | 23,350 | 40,830 | 34,440 | 39,700 |
| Torque | Nm | 31,700 | 55,400 | 46,700 | 53,826 |
| Flow | gal/min | 400-900 | 600-1200 | 400-900 | 400-1000 |
| Range | L/min | 1,510-3,410 | 2,270-4,540 | 1,510-3,410 | 1,514-3,785 |
| Speed Range | RPM | 60-140 | 80-150 | 60-140 | 60-160 |
| Speed | rev/gal | 0.15 | 0.12 | 0.15 | 0.15 |
| Ratio | rev/L | 0.04 | 0.03 | 0.04 | 0.04 |
| Torque Slope | ft-lb/psi | 15.77 | 19.35 | 15.77 | 15.32 |
| | Nm/kPa | 3.10 | 3.81 | 3.10 | 3.01 |

MOTOR SPECIFICATIONS

TITAN22 | PERFORMANCE DRILLING MOTOR

Scientific Drilling's TiTAN22 performance drilling motor is designed for the most extreme drilling environments in the industry. It has been engineered to run with the highest torque power sections, delivering ultimate reliability and durability in all sections of the well.

The TiTAN22 also features a unique Ti-Flex[™] Titanium Flex Shaft and bearing pack assembly to deliver optimal performance in a wide range of applications.

DELIVERING THE ULTIMATE VALUE

- Enhanced WOB capacity, supporting increased and consistent ROP for superior drilling performance
- Rugged driveline design for ultra-high power torque sections, delivering maximized reliability
- Full rotational capabilities in all sections of the well, ensuring optimal wellbore integrity
- Innovative Ti-Flex[™] Titanium Flex Shaft and bearing assembly for increased durability and extended tool life

TARGET APPLICATIONS

- Performance Drilling
- Extended Reach Laterals
- Factory Drilling in Shale Reservoirs
- One Run Applications
- Laminated Formations

TOOL RENDERING

TITAN22 | PERFORMANCE DRILLING MOTOR



TiTAN22 | 5.00" 7/8 3.1

| GENERALS | SPECIFICATIONS |
|-----------------------------|---------------------------------------|
| OD | 5.00 in (127 mm) |
| Length | 30.9 ft (9.42 m) |
| Recommended Hole Sizes | 6 - 6 ¼ in (152 - 159 mm) |
| Max Bend Angle | 2.38° |
| BEARI | NG SECTION |
| Bit to Bend Length | 40.6 in (1.031 m) |
| Bit Box Connection | 3½ API Reg. |
| Max WOB | 30,000 lbs (13,345 DaN) |
| Max Overpull for Rerun | 60,000 lbs (26,689 DaN) |
| Overpull to Yield Motor | 120,000 lbs (53,379 DaN) |
| Max Bit Pressure Drop | 750 psi (5,171 kPa) |
| Opt Bit Pressure Drop | 100 - 600 psi (690 - 4,136 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | RSECTION |
| Lobe Configuration | 7/8 |
| Stages | 3.1 |
| Max Differential Pressure | 700 psi (4,810 kPa) |
| Stall Differential Pressure | 1,050 psi (7,210 kPa) |
| Torque at Max Diff Pressure | 5,460 ft-lbs (7,402 Nm) |
| Stall Torque | 8,190 ft-lbs (11,104 Nm) |
| Flow Range | 150 - 275 gal/min (570 - 1,041 L/min) |
| Speed Range | 47 - 95 RPM |
| Speed Ratio | 0.32 rev/gal (0.08 rev/L) |
| Torque Slope | 7.83 ft-lb/psi (1.54 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 5.00" 7/8 3.1



PERFORMANCE CURVE

TiTAN22 | 5.00" 7/8 3.1



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.

ROTATIONAL LIMIT

TiTAN22 | 5.00"

6" WELLBORE



6¹/₈" WELLBORE



6 ¼" WELLBORE



Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 5.00" 7/8 3.8

| GENERAL S | SPECIFICATIONS |
|-----------------------------|-------------------------------------|
| OD | 5.00 in (127 mm) |
| Length | 27 ft (8.22 m) |
| Recommended Hole Sizes | 6 - 6 ¼ in (152 - 159 mm) |
| Max Bend Angle | 2.38° |
| BEARI | NG SECTION |
| Bit to Bend Length | 40.6 in (1.031 m) |
| Bit Box Connection | 3½ API Reg. |
| Max WOB | 30,000 lbs (13,345 DaN) |
| Max Overpull for Rerun | 60,000 lbs (26,689 DaN) |
| Overpull to Yield Motor | 120,000 lbs (53,379 DaN) |
| Max Bit Pressure Drop | 750 psi (5,171 kPa) |
| Opt Bit Pressure Drop | 100 - 600 psi (690 - 4,136 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 7/8 |
| Stages | 3.8 |
| Max Differential Pressure | 900 psi (6,200 kPa) |
| Stall Differential Pressure | 1,410 psi (9,700 kPa) |
| Torque at Max Diff Pressure | 4,130 ft-lbs (5,600 Nm) |
| Stall Torque | 6,500 ft-lbs (8,900 Nm) |
| Flow Range | 100 - 250 gal/min (380 - 950 L/min) |
| Speed Range | 50 - 140 RPM |
| Speed Ratio | 0.54 rev/gal (0.14 rev/L) |
| Torque Slope | 4.62 ft-lb/psi (0.91 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 5.00" 7/8 3.8



PERFORMANCE CURVE

TiTAN22 | 5.00" 7/8 3.8



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.



ROTATIONAL LIMIT

TiTAN22 | 5.00"



Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 5.00" 7/8 5.0

| GENERALS | SPECIFICATIONS |
|-----------------------------|---------------------------------------|
| OD | 5.00 in (127 mm) |
| Length | 27.9 ft (8.50 m) |
| Recommended Hole Sizes | 6 - 6 ¼ in (152 - 159 mm) |
| Max Bend Angle | 2.38° |
| BEARI | NG SECTION |
| Bit to Bend Length | 40.6 in (1.031 m) |
| Bit Box Connection | 3½ API Reg. |
| Max WOB | 30,000 lbs (13,345 DaN) |
| Max Overpull for Rerun | 60,000 lbs (26,689 DaN) |
| Overpull to Yield Motor | 120,000 lbs (53,379 DaN) |
| Max Bit Pressure Drop | 750 psi (5,171 kPa) |
| Opt Bit Pressure Drop | 100 - 600 psi (690 - 4,136 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 7/8 |
| Stages | 5.0 |
| Max Differential Pressure | 1,180 psi (8,200 kPa) |
| Stall Differential Pressure | 1,860 psi (11,800 kPa) |
| Torque at Max Diff Pressure | 4,670 ft-lbs (6,400 Nm) |
| Stall Torque | 7,350 ft-lbs (10,000 Nm) |
| Flow Range | 150 - 300 gal/min (570 - 1,140 L/min) |
| Speed Range | 90 - 190 RPM |
| Speed Ratio | 0.62 rev/gal (0.16 rev/L) |
| Torque Slope | 3.97 ft-lb/psi (0.78 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 5.00" 7/8 5.0



PERFORMANCE CURVE

TiTAN22 | 5.00" 7/8 5.0



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/- 5 ft of the slide length, as well as in the slide length.

ROTATIONAL LIMIT

TiTAN22 | 5.00"

6" WELLBORE



6¹/₈" WELLBORE



6 ¼" WELLBORE



Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 5.15" 6/7 6.6

| GENERALS | SPECIFICATIONS |
|-----------------------------|---------------------------------------|
| OD | 5.15 in (131 mm) |
| Length | 36.12 ft (11.01 m) |
| Recommended Hole Sizes | 6 - 6 ¾ in (152 - 171 mm) |
| Max Bend Angle | 2.38° |
| BEARI | NG SECTION |
| Bit to Bend Length | 45 in (1.143 m) |
| Bit Box Connection | 3½ API Reg. |
| Max WOB | 30,000 lbs (13,345 DaN) |
| Max Overpull for Rerun | 60,000 lbs (26,689 DaN) |
| Overpull to Yield Motor | 120,000 lbs (53,379 DaN) |
| Max Bit Pressure Drop | 750 psi (5,171 kPa) |
| Opt Bit Pressure Drop | 100 - 600 psi (690 - 4,136 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 6/7 |
| Stages | 6.6 |
| Max Differential Pressure | 1,560 psi (10,700 kPa) |
| Stall Differential Pressure | 2,450 psi (16,900 kPa) |
| Torque at Max Diff Pressure | 8,550 ft-lbs (11,592 Nm) |
| Stall Torque | 13,460 ft-lbs (18,249 Nm) |
| Flow Range | 200 - 400 gal/min (760 - 1,514 L/min) |
| Speed Range | 90 - 180 RPM |
| Speed Ratio | 0.46 rev/gal (0.12 rev/L) |
| Torque Slope | 5.51 ft-lb/psi (1.08 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 5.15" 6/7 6.6



PERFORMANCE CURVE

TiTAN22 | 5.15" 6/7 6.6



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.



ROTATIONAL LIMIT

TiTAN22 | 5.15"



Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 5.15" 6/7 8.0

| GENERALS | SPECIFICATIONS |
|-----------------------------|---------------------------------------|
| OD | 5.15 in (131 mm) |
| Length | 32.8 ft (9.99 m) |
| Recommended Hole Sizes | 6 - 6 ³/4 in (152 - 171 mm) |
| Max Bend Angle | 2.38° |
| BEARI | NG SECTION |
| Bit to Bend Length | 45 in (1.143 m) |
| Bit Box Connection | 3½ API Reg. |
| Max WOB | 30,000 lbs (13,345 DaN) |
| Max Overpull for Rerun | 60,000 lbs (26,689 DaN) |
| Overpull to Yield Motor | 120,000 lbs (53,379 DaN) |
| Max Bit Pressure Drop | 750 psi (5,171 kPa) |
| Opt Bit Pressure Drop | 100 - 600 psi (690 - 4,136 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 6/7 |
| Stages | 8.0 |
| Max Differential Pressure | 1,880 psi (13,000 kPa) |
| Stall Differential Pressure | 2,970 psi (20,500 kPa) |
| Torque at Max Diff Pressure | 6,110 ft-lbs (8,300 Nm) |
| Stall Torque | 9,630 ft-lbs (13,100 Nm) |
| Flow Range | 150 - 350 gal/min (570 - 1,320 L/min) |
| Speed Range | 120-280 RPM |
| Speed Ratio | 0.79 rev/gal (0.20 rev/L) |
| Torque Slope | 3.25 ft-lb/psi (0.64 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 5.15" 6/7 8.0





TiTAN22 | 5.15" 6/7 8.0



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.

ROTATIONAL LIMIT TITAN22 | 5.15"

6" WELLBORE



6 ¹/₈" WELLBORE



6 ¼" WELLBORE



Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 5.15" 6/7 10.4

| GENERALS | SPECIFICATIONS |
|-----------------------------|---------------------------------------|
| OD | 5.15 in (131 mm) |
| Length | 36.56 ft (11.14 m) |
| Recommended Hole Sizes | 6 - 6 ¾ in (152 - 171 mm) |
| Max Bend Angle | 2.38° |
| BEARI | NG SECTION |
| Bit to Bend Length | 45 in (1.14 m) |
| Bit Box Connection | 3½ API Reg. |
| Max WOB | 30,000 lbs (13,345 DaN) |
| Max Overpull for Rerun | 60,000 lbs (26,689 DaN) |
| Overpull to Yield Motor | 120,000 lbs (53,379 DaN) |
| Max Bit Pressure Drop | 750 psi (5,171 kPa) |
| Opt Bit Pressure Drop | 100 - 600 psi (690 - 4,136 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 6/7 |
| Stages | 10.4 |
| Max Differential Pressure | 2,340 psi (16,130 kPa) |
| Stall Differential Pressure | 3,510 psi (24,200 kPa) |
| Torque at Max Diff Pressure | 8,610 ft-lbs (11,673 Nm) |
| Stall Torque | 12,920 ft-lbs (17,517 Nm) |
| Flow Range | 225 - 425 gal/min (852 - 1,608 L/min) |
| Speed Range | 157 - 300 RPM |
| Speed Ratio | 0.70 rev/gal (0.19 rev/L) |
| Torque Slope | 3.68 ft-lb/psi (0.72 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 5.15" 6/7 10.4



PERFORMANCE CURVE

TiTAN22 | 5.15" 6/7 10.4



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.



ROTATIONAL LIMIT

TiTAN22 | 5.15"



Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 6.60" 4/5 7.0

| GENERAL SPECIFICATIONS | | |
|-----------------------------|---|--|
| OD | 6.60 in (168 mm) | |
| Length | 30.9 ft (9.41 m) | |
| Recommended Hole Sizes | 7 ⁷ / ₈ - 8 ³ / ₄ in (200 - 222 mm) | |
| Max Bend Angle | 2.38° | |
| BEARI | NG SECTION | |
| Bit to Bend Length | 49 in (1.244 m) | |
| Bit Box Connection | 4½ API Reg. | |
| Max WOB | 60,000 lbs (26,689 DaN) | |
| Max Overpull for Rerun | 105,000 lbs (46,706 DaN) | |
| Overpull to Yield Motor | 210,000 lbs (93,413 DaN) | |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) | |
| Opt Bit Pressure Drop | 100 - 750 psi (690 - 5,171 kPa) | |
| LCM Capability | 40 lb nut plug | |
| POWE | R SECTION | |
| Lobe Configuration | 4/5 | |
| Stages | 7.0 | |
| Max Differential Pressure | 1,650 psi (11,400 kPa) | |
| Stall Differential Pressure | 2,600 psi (17,900 kPa) | |
| Torque at Max Diff Pressure | 8,820 ft-lbs (12,000 Nm) | |
| Stall Torque | 13,890 ft-lbs (18,900 Nm) | |
| Flow Range | 300-600 gal/min (1,140 - 2,270 L/min) | |
| Speed Range | 150 - 300 RPM | |
| Speed Ratio | 0.49 rev/gal (0.13 rev/L) | |
| Torque Slope | 5.36 ft-lb/psi (1.05 Nm/kPa) | |

GENERAL DIMENSIONS

TiTAN22 | 6.60" 4/5 7.0



PERFORMANCE CURVE

TiTAN22 | 6.60" 4/5 7.0



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/- 5 ft of the slide length, as well as in the slide length.

ROTATIONAL LIMIT TITAN22 | 6.60"

7[%] WELLBORE



8¹/₂" WELLBORE



8³/₄" WELLBORE


TiTAN22 | 6.60" 5/6 8.3

| GENERAL | SPECIFICATIONS |
|-----------------------------|---|
| OD | 6.60 in (168 mm) |
| Length | 38.5 ft (11.73 m) |
| Recommended Hole Sizes | 7 ⁷ /8 - 8 ³ /4 in (200 - 222 mm) |
| Max Bend Angle | 2.38° |
| BEARI | NG SECTION |
| Bit to Bend Length | 49 in (1.244 m) |
| Bit Box Connection | 4½ API Reg. |
| Max WOB | 60,000 lbs (26,689 DaN) |
| Max Overpull for Rerun | 105,000 lbs (46,706 DaN) |
| Overpull to Yield Motor | 210,000 lbs (93,413 DaN) |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) |
| Opt Bit Pressure Drop | 100 - 750 psi (690 - 5,171 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 5/6 |
| Stages | 8.3 |
| Max Differential Pressure | 1,960 psi (13,500 kPa) |
| Stall Differential Pressure | 3,080 psi (21,200 kPa) |
| Torque at Max Diff Pressure | 13,030 ft-lbs (17,700 Nm) |
| Stall Torque | 20,530 ft-lbs (27,900 Nm) |
| Flow Range | 350-750 gal/min (1,320 - 2,840 L/min) |
| Speed Range | 130 - 290 RPM |
| Speed Ratio | 0.38 rev/gal (0.10 rev/L) |
| Torque Slope | 6.68 ft-lb/psi (1.31 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 6.60" 5/6 8.3



TiTAN22 | 6.60" 5/6 8.3



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/- 5 ft of the slide length, as well as in the slide length.

ROTATIONAL LIMIT TITAN22 | 6.60"

7[%] WELLBORE



8¹/₂" WELLBORE



8³/₄" WELLBORE



TiTAN22 | 6.60" 7/8 3.3

| GENERALS | SPECIFICATIONS |
|-----------------------------|---------------------------------------|
| OD | 6.60 in (168 mm) |
| Length | 33.8 ft (10.3 m) |
| Recommended Hole Sizes | 7 7/8 - 8 3/4 in (200 - 222 mm) |
| Max Bend Angle | 2.38° |
| BEARI | NG SECTION |
| Bit to Bend Length | 49 in (1.244 m) |
| Bit Box Connection | 4½ API Reg. |
| Max WOB | 60,000 lbs (26,689 DaN) |
| Max Overpull for Rerun | 105,000 lbs (46,706 DaN) |
| Overpull to Yield Motor | 210,000 lbs (93,413 DaN) |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) |
| Opt Bit Pressure Drop | 100 - 750 psi (690 - 5,171 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 7/8 |
| Stages | 3.3 |
| Max Differential Pressure | 780 psi (5,400 kPa) |
| Stall Differential Pressure | 1,230 psi (8,500 kPa) |
| Torque at Max Diff Pressure | 13,150 ft-lbs (17,900 Nm) |
| Stall Torque | 20,710 ft-lbs (28,100 Nm) |
| Flow Range | 300-600 gal/min (1,140 - 2,270 L/min) |
| Speed Range | 50 - 90 RPM |
| Speed Ratio | 0.15 rev/gal (0.04 rev/L) |
| Torque Slope | 16.95 ft-lb/psi (3.33 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 6.60" 7/8 3.3



TiTAN22 | 6.60" 7/8 3.3



^{*(}Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.

ROTATIONAL LIMIT TiTAN22 | 6.60"

7⁷/₈" WELLBORE



8¹/₂" WELLBORE



8³/₄" WELLBORE



Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 6.60" 7/8 5.0

| GENERAL S | SPECIFICATIONS |
|-----------------------------|---------------------------------------|
| OD | 6.60 in (168 mm) |
| Length | 29.6 ft (9.02 m) |
| Recommended Hole Sizes | 7 7/8 - 8 3/4 in (200 - 222 mm) |
| Max Bend Angle | 2.38° |
| BEARI | NG SECTION |
| Bit to Bend Length | 49 in (1.244 m) |
| Bit Box Connection | 4½ API Reg. |
| Max WOB | 60,000 lbs (26,689 DaN) |
| Max Overpull for Rerun | 105,000 lbs (46,706 DaN) |
| Overpull to Yield Motor | 210,000 lbs (93,413 DaN) |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) |
| Opt Bit Pressure Drop | 100 - 750 psi (690 - 5,171 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 7/8 |
| Stages | 5.0 |
| Max Differential Pressure | 1,180 psi (8,200 kPa) |
| Stall Differential Pressure | 1,860 psi (12,800 kPa) |
| Torque at Max Diff Pressure | 10,650 ft-lbs (14,500 Nm) |
| Stall Torque | 16,770 ft-lbs (22,800 Nm) |
| Flow Range | 300-650 gal/min (1,140 - 2,460 L/min) |
| Speed Range | 80 - 188 RPM |
| Speed Ratio | 0.29 rev/gal (0.08 rev/L) |
| Torque Slope | 9.06 ft-lb/psi (1.78 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 6.60" 7/8 5.0







For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/- 5 ft of the slide length, as well as in the slide length.

ROTATIONAL LIMIT TITAN22 | 6.60"

7⁷/₈" WELLBORE



8¹/₂" WELLBORE



8³/₄" WELLBORE



Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 6.60" 7/8 6.4

| GENERALS | SPECIFICATIONS |
|-----------------------------|---------------------------------------|
| OD | 6.60 in (168 mm) |
| Length | 33.8 ft (10.3 m) |
| Recommended Hole Sizes | 7 7/8 - 8 3/4 in (200 - 222 mm) |
| Max Bend Angle | 2.38° |
| BEARI | NG SECTION |
| Bit to Bend Length | 49 in (1.244 m) |
| Bit Box Connection | 4½ API Reg. |
| Max WOB | 60,000 lbs (26,689 DaN) |
| Max Overpull for Rerun | 105,000 lbs (46,706 DaN) |
| Overpull to Yield Motor | 210,000 lbs (93,413 DaN) |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) |
| Opt Bit Pressure Drop | 100 - 750 psi (690 - 5,171 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 7/8 |
| Stages | 6.4 |
| Max Differential Pressure | 1,510 psi (10,400 kPa) |
| Stall Differential Pressure | 2,370 psi (16,400 kPa) |
| Torque at Max Diff Pressure | 13,360 ft-lbs (18,500 Nm) |
| Stall Torque | 21,470 ft-lbs (29,100 Nm) |
| Flow Range | 300-650 gal/min (1,140 - 2,460 L/min) |
| Speed Range | 80 - 188 RPM |
| Speed Ratio | 0.29 rev/gal (0.08 rev/L) |
| Torque Slope | 9.06 ft-lb/psi (1.78 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 6.60" 7/8 6.4







*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.

ROTATIONAL LIMIT

TiTAN22 | 6.60"

7[%]" WELLBORE



8¹/₂" WELLBORE



8³/₄" WELLBORE



Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 7.15" 5/6 8.3

| GENERAL S | SPECIFICATIONS |
|-----------------------------|-------------------------------------|
| OD | 7.15 in (181 mm) |
| Length | 39.2 ft (11.94 m) |
| Recommended Hole Sizes | 8 1/2 - 9 7/8 in (215 - 250 mm) |
| Max Bend Angle | 2.12° |
| BEARII | NG SECTION |
| Bit to Bend Length | 57 in (1.44 m) |
| Bit Box Connection | 4½ in API Reg. Box |
| Max WOB | 60,000 lbs (26,689 DaN) |
| Max Overpull for Rerun | 110,000 lbs (48,930 DaN) |
| Overpull to Yield Motor | 240,000 lbs (106,757 DaN) |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) |
| Opt Bit Pressure Drop | 100 - 750 psi (690 - 5,171 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 5/6 |
| Stages | 8.3 |
| Max Differential Pressure | 1,960 psi (13,500 kPa) |
| Stall Differential Pressure | 3,080 ft-lbs (21,200 Nm) |
| Torque at Max Diff Pressure | 13,030 ft-lbs (17,700 Nm) |
| Stall Torque | 20,530 ft-lbs (27,900 Nm) |
| Flow Range | 350-750 gal/min (1,320-2,840 L/min) |
| Speed Range | 130 - 290 RPM |
| Speed Ratio | 0.38 rev/gal (0.10 rev/L) |
| Torque Slope | 6.68 ft-lb/psi (1.31 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 7.15" 5/6 8.3



TiTAN22 | 7.15" 5/6 8.3



ROTATIONAL LIMIT TITAN22 | 7.15"

8¹/₂" WELLBORE



8³/₄" WELLBORE



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.

Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 7.15" 5/6 11.2

| GENERALS | SPECIFICATIONS |
|-----------------------------|---------------------------------------|
| OD | 7.15 in (181 mm) |
| Length | 42.5 ft (12.95 m) |
| Recommended Hole Sizes | 8 1/2 - 9 7/8 in (215 - 250 mm) |
| Max Bend Angle | 2.12° |
| BEARI | NG SECTION |
| Bit to Bend Length | 57 in (1.44 m) |
| Bit Box Connection | 4½ in API Reg. Box |
| Max WOB | 60,000 lbs (26,689 DaN) |
| Max Overpull for Rerun | 110,000 lbs (48,930 DaN) |
| Overpull to Yield Motor | 240,000 lbs (106,757 DaN) |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) |
| Opt Bit Pressure Drop | 100 - 750 psi (690 - 5,171 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 5/6 |
| Stages | 11.2 |
| Max Differential Pressure | 2,520 psi (17,374 kPa) |
| Stall Differential Pressure | 3,780 psi (26,060 kPa) |
| Torque at Max Diff Pressure | 16,420 ft-lbs (22,260 Nm) |
| Stall Torque | 24,630 ft-lbs (33,393 Nm) |
| Flow Range | 450-750 gal/min (1,703 - 2,840 L/min) |
| Speed Range | 180 - 300 RPM |
| Speed Ratio | 0.40 rev/gal (0.11 rev/L) |
| Torque Slope | 6.51 ft-lb/psi (1.28 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 7.15" 5/6 11.2



TiTAN22 | 7.15" 5/6 11.2



ROTATIONAL LIMIT TiTAN22 | 7.15"

8¹/₂" WELLBORE



8³/₄" WELLBORE



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.

Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 7.15" 6/7 7.1

| GENERAL SPECIFICATIONS | | |
|-----------------------------|---------------------------------------|--|
| OD | 7.15 in (181 mm) | |
| Length | 42.5 ft (12.95 m) | |
| Recommended Hole Sizes | 8 1/2 - 9 7/8 in (215 - 250 mm) | |
| Max Bend Angle | 2.12° | |
| BEARI | NG SECTION | |
| Bit to Bend Length | 57 in (1.44 m) | |
| Bit Box Connection | 4½ in API Reg. Box | |
| Max WOB | 60,000 lbs (26,689 DaN) | |
| Max Overpull for Rerun | 110,000 lbs (48,930 DaN) | |
| Overpull to Yield Motor | 240,000 lbs (106,757 DaN) | |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) | |
| Opt Bit Pressure Drop | 100 - 750 psi (690 - 5,171 kPa) | |
| LCM Capability | 40 lb nut plug | |
| POWE | R SECTION | |
| Lobe Configuration | 6/7 | |
| Stages | 7.1 | |
| Max Differential Pressure | 1,670 psi (11,600 kPa) | |
| Stall Differential Pressure | 2,630 psi (18,200 kPa) | |
| Torque at Max Diff Pressure | 18,230 ft-lbs (24,716 Nm) | |
| Stall Torque | 28,700 ft-lbs (39,000 Nm) | |
| Flow Range | 350-750 gal/min (1,324 - 2,840 L/min) | |
| Speed Range | 80 - 170 RPM | |
| Speed Ratio | 0.23 rev/gal (0.06 rev/L) | |
| Torque Slope | 10.92 ft-lb/psi (2.15 Nm/kPa) | |

GENERAL DIMENSIONS

TiTAN22 | 7.15" 6/7 7.1



TiTAN22 | 7.15" 6/7 7.1



ROTATIONAL LIMIT TITAN22 | 7.15"

8¹/₂" WELLBORE



8³/₄" WELLBORE



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.

Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 7.15" 7/8 9.4

| GENERALS | SPECIFICATIONS |
|-----------------------------|---------------------------------------|
| OD | 7.15 in (181 mm) |
| Length | 42.5 ft (12.95 m) |
| Recommended Hole Sizes | 8 1/2 - 9 7/8 in (215 - 250 mm) |
| Max Bend Angle | 2.12° |
| BEARI | NG SECTION |
| Bit to Bend Length | 57 in (1.44 m) |
| Bit Box Connection | 4½ in API Reg. Box |
| Max WOB | 60,000 lbs (26,689 DaN) |
| Max Overpull for Rerun | 110,000 lbs (48,930 DaN) |
| Overpull to Yield Motor | 240,000 lbs (106,757 DaN) |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) |
| Opt Bit Pressure Drop | 100 - 750 psi (690 - 5,171 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 7/8 |
| Stages | 9.4 |
| Max Differential Pressure | 2,120 psi (14,580 kPa) |
| Stall Differential Pressure | 3,170 psi (21,870 kPa) |
| Torque at Max Diff Pressure | 18,680 ft-lbs (25,330 Nm) |
| Stall Torque | 28,020 ft-lbs (37,990 Nm) |
| Flow Range | 500-750 gal/min (1,893 - 2,839 L/min) |
| Speed Range | 144 - 216 RPM |
| Speed Ratio | 0.28 rev/gal (0.08 rev/L) |
| Torque Slope | 8.83 ft-lb/psi (1.73 Nm/kPa) |

GENERAL DIMENSIONS

Titan22 | 7.15" 7/8 9.4



TiTAN22 | 7.15" 7/8 9.4



ROTATIONAL LIMIT TITAN22 | 7.15"

8¹/₂" WELLBORE



8³/₄" WELLBORE



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.

Refer to full rotational limits disclaimer in the appendix prior to use

TiTAN22 | 9.15" 7/8 4.0

| GENERALS | SPECIFICATIONS |
|-----------------------------|--|
| OD | 9.15 in. (232.41 mm) |
| Length | 32 ft (9.75 m) |
| Recommended Hole Sizes | 12 ¹ /4-26 in (311.15-660.40 mm) |
| Max Bend Angle | 1.83° |
| BEARI | NG SECTION |
| Bit to Bend Length | 66 in. (1.67 m) |
| Bit Box Connection | 6 $^{\rm 5}/_{\rm 8}$ in., 7 $^{\rm 5}/_{\rm 8}$ in API Reg. Box |
| Max WOB | 120,000 lbs (53,378 DaN) |
| Max Overpull for Rerun | 100,000 lbs (48,930 DaN) |
| Overpull to Yield Motor | 250,000 lbs (111,205 DaN) |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) |
| Opt Bit Pressure Drop | 250-900 psi (1,723-6,205 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | RSECTION |
| Lobe Configuration | 7/8 |
| Stages | 4.0 |
| Max Differential Pressure | 940 psi (6,895 kPa) |
| Stall Differential Pressure | 1,490 psi (10,200 kPa) |
| Torque at Max Diff Pressure | 14,830 ft-lbs (20,100 Nm) |
| Stall Torque | 23,350 ft-lbs (31,700 Nm) |
| Flow Range | 400-900 gal/min (1,510-3,410 L/min) |
| Speed Range | 60 - 140 RPM |
| Speed Ratio | 0.15 rev/gal (0.04 rev/L) |
| Torque Slope | 15.77 ft-lb/psi (3.10 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 9.15" 7/8 4.0



TiTAN22 | 9.15" 7/8 4.0



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.

TiTAN22 | 9.15" 7/8 5.7

| GENERALS | SPECIFICATIONS |
|-----------------------------|--|
| OD | 9.15 in. (232.41 mm) |
| Length | 38.34 ft (11.68 m) |
| Recommended Hole Sizes | 12 ¹ /4-26 in (311.15-660.40 mm) |
| Max Bend Angle | 1.83° |
| BEARI | NG SECTION |
| Bit to Bend Length | 66 in. (1.67 m) |
| Bit Box Connection | 6 $^{5}/_{8}$ in., 7 $^{5}/_{8}$ in API Reg. Box |
| Max WOB | 120,000 lbs (53,378 DaN) |
| Max Overpull for Rerun | 100,000 lbs (48,930 DaN) |
| Overpull to Yield Motor | 250,000 lbs (111,205 DaN) |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) |
| Opt Bit Pressure Drop | 250-900 psi (1,723-6,205 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 7/8 |
| Stages | 5.7 |
| Max Differential Pressure | 1,340 psi (9,300 kPa) |
| Stall Differential Pressure | 2,110 psi (14,600 kPa) |
| Torque at Max Diff Pressure | 25,920 ft-lbs (35,200 Nm) |
| Stall Torque | 40,830 ft-lbs (55,400 Nm) |
| Flow Range | 600-1,200 gal/min (2,270-4,540 L/min) |
| Speed Range | 80 - 150 RPM |
| Speed Ratio | 0.12 rev/gal (0.03 rev/L) |
| Torque Slope | 19.35 ft-lb/psi (3.81 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 9.15" 7/8 5.7



TiTAN22 | 9.15" 7/8 5.7



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.

TiTAN22 | 9.15" 7/8 5.9

| GENERAL SPECIFICATIONS | |
|-----------------------------|---|
| OD | 9.15 in. (232.41 mm) |
| Length | 44.4 ft (13.53 m) |
| Recommended Hole Sizes | 12 ¹ /4-26 in (311.15-660.40 mm) |
| Max Bend Angle | 1.83° |
| BEARI | NG SECTION |
| Bit to Bend Length | 66 in. (1.67 m) |
| Bit Box Connection | 6 $5/_8$ in., 7 $5/_8$ in API Reg. Box |
| Max WOB | 120,000 lbs (53,378 DaN) |
| Max Overpull for Rerun | 100,000 lbs (48,930 DaN) |
| Overpull to Yield Motor | 250,000 lbs (111,205 DaN) |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) |
| Opt Bit Pressure Drop | 250-900 psi (1,723-6,205 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | R SECTION |
| Lobe Configuration | 7/8 |
| Stages | 5.9 |
| Max Differential Pressure | 1,390 psi (9,600 kPa) |
| Stall Differential Pressure | 2,190 psi (15,100 kPa) |
| Torque at Max Diff Pressure | 21,870 ft-lbs (29,700 Nm) |
| Stall Torque | 34,440 ft-lbs (46,700 Nm) |
| Flow Range | 400-900 gal/min (1,510-3,410 L/min) |
| Speed Range | 60 - 140 RPM |
| Speed Ratio | 0.15 rev/gal (0.04 rev/L) |
| Torque Slope | 15.77 ft-lb/psi (3.10 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 9.15" 7/8 5.9



TiTAN22 | 9.15" 7/8 5.9



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.

TiTAN22 | 9.15" 7/8 7.0

| GENERAL | SPECIFICATIONS |
|-----------------------------|---|
| OD | 9.15 in. (232.41 mm) |
| Length | 44.4 ft (13.53 m) |
| Recommended Hole Sizes | 12 ¹ /4-26 in (311.15-660.40 mm) |
| Max Bend Angle | 1.83° |
| BEARI | NG SECTION |
| Bit to Bend Length | 66 in. (1.67 m) |
| Bit Box Connection | 6 $5/_{8}$ in., 7 $5/_{8}$ in API Reg. Box |
| Max WOB | 120,000 lbs (53,378 DaN) |
| Max Overpull for Rerun | 100,000 lbs (48,930 DaN) |
| Overpull to Yield Motor | 250,000 lbs (111,205 DaN) |
| Max Bit Pressure Drop | 1,000 psi (6,894 kPa) |
| Opt Bit Pressure Drop | 250-900 psi (1,723-6,205 kPa) |
| LCM Capability | 40 lb nut plug |
| POWE | RSECTION |
| Lobe Configuration | 7/8 |
| Stages | 7.0 |
| Max Differential Pressure | 1,650 psi (11,376 kPa) |
| Stall Differential Pressure | 2,600 psi (17,926 kPa) |
| Torque at Max Diff Pressure | 25,210 ft-lbs (34,180 Nm) |
| Stall Torque | 39,700 ft-lbs (53,826 Nm) |
| Flow Range | 400-1000 gal/min (1,514-3,785 L/min) |
| Speed Range | 60 - 160 RPM |
| Speed Ratio | 0.15 rev/gal (0.039 rev/L) |
| Torque Slope | 15.32 ft-lb/psi (3.01 Nm/kPa) |

GENERAL DIMENSIONS

TiTAN22 | 9.15" 7/8 7.0



TiTAN22 | 9.15" 7/8 7.0



*(Right) The DLS in the figure represents the local dog-leg.

For Example: If the motor slides for 10 ft and outputs a $15^{\circ}/100$ ft curve over that 10 ft, the local dog-leg (DLS in the figure) is $15^{\circ}/100$ ft. The rotation limits should be adhered to when the bit depth is within +/-5 ft of the slide length, as well as in the slide length.

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TALON II ADJUSTMENT PROCEDURE



- 1. Break Connection
- 2. Place rig tongs on the Upper Housing and on the Torque Sleeve. Break the connection by applying torque in the direction indicated in Fig. 1
- 3. Set ABH Angle
- 4. Holding the Upper Housing stationary, rotate the Lower Housing until the desired angle marks are aligned on the Alignment Ring and the Lower Housing
- 5. Note: Always use the shortest direction to the required bend angle setting
- 6. Make-Up Connection
- 7. Holding the Upper and the Lower Housings stationary, use a chain tong to make-up the Torque Sleeve until it shoulders on the Alignment Ring.
- Place rig tongs on the Upper Housing and on the Torque Sleeve. Torque connection to recommended value by applying torque in the direction indicated in Fig. 2.

TALON II ABH TORQUE VALUES

| Motor Sizo | Tor | que |
|------------|--------|--------|
| wotor Size | ft-lbs | Nm |
| 2-3/8" | 1,250 | 1,694 |
| 2-7/8" | 2,750 | 3,728 |
| 3-3/4" | 5,000 | 6,779 |
| 4-3/4" | 9,000 | 12,202 |
| 6-1/4" | 19,500 | 26,438 |
| 6-1/2" | 26,500 | 35,929 |
| 6-3/4" | 28,500 | 38,640 |
| 8" | 47,500 | 64,401 |
| 9-5/8" | 70,000 | 94,907 |

SHOCK AND VIBRATION LIMITS

| | AX | IAL VIBRATI | ON | |
|------------|------|-------------|-------|-----|
| DD Level | 0 | 1 | 2 | 3 |
| RMS (g) | < 2 | 2 - 4 | 4 - 6 | > 6 |
| Time (hrs) | None | None | 6 | 0.5 |

| | LATE | RAL VIBRA | TION | |
|------------|-------|-----------|---------|-------|
| DD Level | 0 | 1 | 2 | 3 |
| RMS (g) | < 2.5 | 2.5 - 5 | 5 - 7.5 | > 7.5 |
| Time (hrs) | None | None | 6 | 0.5 |

| | | STICK SLIP | | |
|------------|--------|------------|------------|--------|
| DD Level | 0 | 1 | 2 | 3 - 6 |
| RMS (g) | < 100% | 100 - 150% | 150 - 200% | > 200% |
| Time (hrs) | None | None | 6 | 0.5 |

HOLE SIZE RANGE PER MOTOR SIZE

| MOTOR SIZE | RECOM HOLE SIZ | MENDED E RANGE |
|------------|-------------------|-------------------|
| 3 3⁄4" | 4¾" - 5%" | 121 – 149 mm |
| 4¾" | 5 1/8" - 7 1/8" | 149 – 200 mm |
| 6 ¼" | 7 1/8" - 8 3/4" | 200 – 222 mm |
| 6 ½" | 7 1/8" - 9 1/8" | 200 – 251 mm |
| 6 ¾" | 8 1⁄2" - 9 7⁄8" | 216 – 251 mm |
| 7 ¼" | 8 ½" – 9 ¾" | 216 – 251 mm |
| 8" | 9½" – 12½" | 241 – 318 mm |
| 9 5⁄8" | 12¼" - 26" | 311 – 660 mm |

PREDICTED BUILD RATE

housing. Since other factors, such as formation, bit type, WOB, hole gauge, etc. affect the actual build rate, the following numbers should be used as a guide only. Note: the expected build rates are for slick assemblies, and the use of stabilizers will affect the The following tables predict the average build rate based on the size of the motor, hole size, and the bend angle of the drive shaft dogleg expectancy.

| | 3.00 | | 26.1 | 25.0 | |
|-------|------------------|------------|--------|--------|--|
| | 2.75 | | 23.3 | 22.3 | |
| | 2.50 | | 20.8 | 19.9 | |
| | 2.25 | | 18.4 | 17.2 | |
| | 2.00 | 00 ft) | 15.9 | 15.1 | |
| | 1.75 | ate (deg/1 | 13.5 | 12.8 | |
| | 1.50 | ed Build R | 11.2 | 10.5 | |
| Motor | 1.25 | Expecte | 8.5 | 7.9 | |
| 3¾" | 1.00 | | 6.1 | 5.5 | |
| | 0.75 | | 3.8 | 3.7 | |
| | 0.50 | | 2.7 | 2.6 | |
| | 0.25 | | N/A | N/A | |
| | Bend Angle (Deg) | Hole Size | 4 3⁄4" | 5 7/8" | |

| | 3.00 | | 24.5 | 23.7 | 23.3 | 21.8 | 17.4 |
|---------|---------------------------|------------|--------|--------|--------|--------|-------------------|
| | 2.75 | | 22.0 | 21.2 | 20.8 | 19.5 | 15.3 |
| | 2.50 | | 19.6 | 18.8 | 18.5 | 17.0 | 12.7 |
| | 2.25 | | 17.2 | 16.4 | 16.1 | 14.7 | 11.6 |
| | 2.00 | 1 00 ft) | 14.3 | 13.7 | 13.4 | 12.4 | 11.0 |
| | 1.75 | late (deg/ | 12.5 | 12.0 | 11.8 | 10.9 | 9.6 |
| | 1.50 | ed Build F | 10.8 | 10.4 | 10.2 | 9.4 | 8.3 |
| " Motor | " Motor 1.25 Expect | Expect | 0.6 | 8.6 | 8.4 | 7.8 | 6.9 |
| 4 34 | 1.00 | | 7.2 | 7.0 | 6.8 | 6.3 | 5.5 |
| | 0.50 0.75 | | 5.4 | 5.2 | 5.1 | 4.7 | 4.2 |
| | | 3.6 | 3.4 | 3.3 | 3.1 | 2.8 | |
| | 0.25 | | 1.8 | 1.7 | 1.6 | 1.5 | 1.4 |
| | Bend Angle (Deg) | Hole Size | 5 7/8" | 6 1⁄8" | 6 1/4" | 6 3/4" | 7 ₇₈ " |

PREDICTED BUILD RATE (CONTINUED)

| | | | | 6 ¼' | ' Motor | | | | | | | |
|------------------|------|------|------|----------|---------|------------|------------|----------|------|------|------|------|
| Bend Angle (Deg) | 0.25 | 0.50 | 0.75 | 1.00 | 1.25 | 1.50 | 1.75 | 2.00 | 2.25 | 2.50 | 2.75 | 3.00 |
| Hole Size | | | | | Expect | ed Build F | late (deg/ | 1 00 ft) | | | | |
| 7 7⁄8" | N/A | 1.2 | 2.5 | 4.2 | 6.0 | 7.7 | 9.5 | 11.2 | 13.0 | 14.6 | 16.5 | 18.2 |
| 8 1⁄2 " | N/A | N/A | 1.5 | 3.2 | 4.9 | 6.7 | 8.4 | 10.2 | 11.9 | 13.7 | 15.4 | 17.2 |
| 8 3/4" | N/A | N/A | 1.0 | 2.8 | 4.5 | 6.3 | 8.0 | 9.8 | 11.5 | 13.3 | 15.0 | 16.8 |
| | | | | | | | | | | | | |
| | | | | 6 ½" and | 6∛4" Mo | otor | | | | | | |

| | | | | 6 ½" and | I 6 ¾" Md | otor | | | | | | |
|---------------------|------|------|------|----------|-----------|------------|------------|----------|------|------|------|------|
| Bend Angle (Deg) | 0.25 | 0.50 | 0.75 | 1.00 | 1.25 | 1.50 | 1.75 | 2.00 | 2.25 | 2.50 | 2.75 | 3.00 |
| Hole Size | | | | | Expect | ed Build F | late (deg/ | 1 00 ft) | | | | |
| 7 7⁄8" (61⁄2" only) | 1.5 | 2.9 | 4.3 | 5.7 | 7.1 | 8.5 | 9.9 | 11.3 | 13.2 | 15.1 | 17.0 | 18.9 |
| 8 1/2 " & 8 3/4 " | 1.4 | 2.8 | 4.2 | 5.6 | 7.0 | 8.4 | 9.8 | 11.2 | 13.1 | 15.0 | 16.9 | 18.8 |
| 9 ½" | 1.2 | 2.5 | 3.7 | 5.0 | 6.2 | 7.5 | 8.7 | 9.9 | 11.1 | 12.3 | 13.5 | 14.7 |
| , ⁸ /26 | 1.2 | 2.4 | 3.6 | 4.8 | 6.0 | 7.2 | 8.4 | 9.5 | 10.6 | 11.7 | 12.8 | 13.9 |

| NUED |
|---------|
| CONTIN |
| RATE ((|
| BUILD |
| ICTED |
| PRED |

| | 3.00 | | 15.8 | 14.7 | 14.4 | | | | | | |
|-------|------------------|------------|---------|----------|--------|-----|-----|--|-----|-----|-----|
| | 2.75 | | 14.4 | 13.3 | 13.0 | | | | | | |
| | 2.50 | | 13.0 | 12.0 | 11.6 | | | | | | |
| | 2.25 | | 11.5 | 10.4 | 10.2 | | | | | | |
| | 2.00 | 1 00 ft) | 10.1 | 9.0 | 8.6 | | | | | | |
| | 1.75 | ate (deg/1 | 8.7 | 7.6 | 7.2 | | | | | | |
| | 1.50 | ed Build R | 7.3 | 6.2 | 5.8 | | | | | | |
| Motor | 1.25 | Expected | Expecte | Expected | 5.9 | 4.8 | 4.4 | | | | |
| 714" | 1.00 | | 4.4 | 3.3 | 2.9 | | | | | | |
| | 0.75 | | | | | | | | 2.9 | 1.9 | 1.5 |
| | 0.50 | | | | | | | | | | |
| | 0.25 | | N/A | N/A | N/A | | | | | | |
| | Bend Angle (Deg) | Hole Size | 8 ½" | 9 ½" | 9 7⁄8" | | | | | | |

| | 3.00 | | 15.9 | 15.3 | 10.5 | |
|------------|------------------|------------|------|---------|-------|--|
| | 2.75 | | 14.5 | 13.8 | 9.1 | |
| | 2.50 | | 13.0 | 12.3 | 7.6 | |
| | 2.25 | | 11.6 | 10.9 | 6.2 | |
| | 2.00 | 1 00 ft) | 10.1 | 9.4 | 4.7 | |
| | 1.75 | late (deg/ | 8.6 | 8.0 | 3.2 | |
| | 1.50 | ed Build R | 7.2 | 6.5 | 1.8 | |
| Motor | 1.25 | Expect | 5.7 | 5.0 | N/A | |
| * 8 | 1.00 | | 4.3 | 3.6 | N/A | |
| | 0.75 | | 2.8 | 2.1 | N/A | |
| | 0.50 | | 1.3 | N/A | N/A | |
| | 0.25 | | N/A | N/A | N/A | |
| | Bend Angle (Deg) | Hole Size | 9 ½" | 9 7/8 " | 12 ½" | |

PREDICTED BUILD RATE (CONTINUED)

| · | 3.00 | | 10.0 | 8.1 | 6.8 | 5.4 | 4.4 |
|----------------|------------------|-------------------------|-------|----------|-------|-----|-----|
| | 2.75 | | 9.2 | 7.4 | 6.2 | 4.9 | 4.1 |
| | 2.50 | | 8.3 | 6.7 | 5.7 | 4.4 | 3.7 |
| | 2.25 | | 7.5 | 6.1 | 5.1 | 4.0 | 3.3 |
| | 2.00 | 1 00 ft) | 6.7 | 5.5 | 4.5 | 3.5 | 3.0 |
| | 1.75 | tate (deg/ ⁻ | 5.8 | 4.8 | 4.0 | 3.1 | 2.6 |
| | 1.50 | ed Build R | 5.0 | 4.1 | 3.4 | 2.6 | 2.2 |
| ' Motor | 1.25 | Expect | 4.2 | 3.4 | 2.8 | 2.2 | 1.9 |
| -8∕ <u>-</u> 6 | 1.00 | | 3.3 | 2.8 | 2.3 | 1.8 | 1.5 |
| | 0.75 | | 2.5 | 2.1 | 1.7 | 1.3 | 1.1 |
| | 0.50 | | 1.7 | 1.4 | 1.1 | 0.8 | 0.7 |
| | 0.25 | | 0.8 | 0.7 | 0.6 | 0.4 | 0.4 |
| | Bend Angle (Deg) | Hole Size | 12 ¼" | 14 3/4 " | 17 ½" | 22" | 26" |

HOLE CURVATURE CALCULATION

The following table shows the radius of curvature for different build rates. These numbers are generated by using the Radius Formula.

R = MD ÷ (0.017453 x Angle) VD = R Sin (Angle) HD = R [1-Cos (Angle)]



| Build Rate | Hole Radius | | Build Rate | Ho Rao | ole dius |
|---------------|----------------|-----|---------------|-----------|-------------|
| °/100 ft | ft | m | °/100 ft | ft | m |
| 2 | 2,865 | 873 | 66 | 87 | 27 |
| 4 | 1,432 | 436 | 68 | 84 | 26 |
| 6 | 955 | 291 | 70 | 82 | 25 |
| 8 | 716 | 218 | 72 | 80 | 24 |
| 10 | 573 | 175 | 74 | 77 | 23 |
| 12 | 477 | 145 | 76 | 75 | 23 |
| 14 | 409 | 125 | 78 | 73 | 22 |
| 16 | 358 | 109 | 80 | 72 | 22 |
| 18 | 318 | 97 | 82 | 70 | 21 |
| 20 | 286 | 87 | 84 | 68 | 21 |
| 22 | 260 | 79 | 86 | 67 | 20 |
| 24 | 239 | 73 | 88 | 65 | 20 |
| 26 | 220 | 67 | 90 | 64 | 20 |
| 28 | 205 | 62 | 92 | 62 | 19 |
| 30 | 191 | 58 | 94 | 61 | 19 |
| 32 | 179 | 55 | 96 | 60 | 18 |
| 34 | 169 | 52 | 98 | 58 | 18 |
| 36 | 159 | 48 | 100 | 57 | 17 |
| 38 | 151 | 46 | 105 | 55 | 17 |
| 40 | 143 | 44 | 110 | 52 | 16 |
| 42 | 136 | 41 | 115 | 50 | 15 |
| 44 | 130 | 40 | 120 | 48 | 15 |
| 46 | 125 | 38 | 125 | 46 | 14 |
| 48 | 119 | 36 | 130 | 44 | 13 |
| 50 | 115 | 35 | 135 | 42 | 13 |
| 52 | 110 | 34 | 140 | 41 | 13 |
| 54 | 100 | 30 | 145 | 40 | 12 |
| 56 | 102 | 31 | 150 | 38 | 12 |
| 58 | 99 | 30 | 155 | 37 | 11 |
| 60 | 95 | 29 | 160 | 36 | 11 |
| 62 | 92 | 28 | 165 | 35 | 11 |
| 64 | 90 | 27 | 170 | 34 | 10 |
| | | | | | |

FORMULAS

Horsepower

| BHP = | $\frac{P_{b} x Q}{1714}$ | BHP = Bit Hydraulic Horsepower (HP) P _b = Bit Pressure Drop (psi) Q = Flow Rate (gal/min) |
|--------|--------------------------|--|
| MHP = | <u>T x N</u> 5252 | MHP = Mechanical Horsepower (HP) T = Torque (ft-lb) N = Motor RPM |
| AHHP = | <u>P x Q</u> 1714 | AHHP = Available Hydraulic Horsepower to Motor (HP) P = Motor Pressure Drop (psi) Q = Flow Rate (gal/min) |

Pressure

| $\mathbf{Pb} = \frac{\mathbf{Q}^2 \mathbf{x} \mathbf{W}}{10856 \mathbf{x} \mathrm{TFA}^2}$ | Pb = Bit Pressure Drop (psi) Q = Flow Rate (gal/min) W = Mud Weight (lb/gal) TFA = Total Flow Area (in ²) |
|--|---|
| $\mathbf{Ph} = \begin{array}{c} 0.052 \text{ x TVD} \\ \text{x W} \end{array}$ | Ph = Hydrostatic Pressure TVD = Total Vertical Depth (ft) W = Mud Weight (lb/gal) |
| PNC = $\frac{P_{oc} \times W_{New}}{W_{old}}$ | PNC = New Circulating Pressure Due to Change in Mud Weight P _{OC} = Old Circulating Pressure (psi) W _{New} = New Mud Weight (lb/gal) W _{Old} = Old Mud Weight (lb/gal) |

Velocity

| AV = $\frac{0.4085 \text{ x Q}}{\text{D}_{\text{h}}^2 - \text{D}_{\text{S}}^2}$ | AV = Annular Velocity (ft/sec) Q = Flow Rate (gal/min) D_h = Hole Diameter (in) D_S = Drill string OD (in) |
|--|---|
| ••••• | •••••• |
| $\mathbf{NV} = \frac{0.3209 \times Q}{A}$ | NV = Nozzle Fluid Velocity (ft/sec) Q = Flow Rate (gal/min) A = Nozzle Area (in²) |

Air Motor RPM Calculation

| RPM _{Motor} = | RPM _{Foam} + RPM _{Air} |
|---------------------------|--|
| RPM _{Foam} = | (rev/gal) x (gal/min) _{Foam} |
| RPM _{Air} = | [0.21 x SCFM x (460 + BHCT) x (rev/gal) |
| | I |
| RPM _{Foam} = | Motor RPM due to flow of foam |
| RPM _{Air} = | Motor RPM due to air flow |
| rev/gal = | Derived from motor specification sheets |
| gal/min _{Foam} = | Volumetric flow rate of foam (gal/min) |
| SCFM = | Compressor input flow rate (before pressurizing) |
| BHCT = | Bottom Hole Circulating Temperature (F°) |
| P = | Exit pressure at the compressor (psi) |

Other Useful Formulas

| Hole Area = (in²) | $\frac{3.1416 \text{ x } {D_h}^2}{4}$ | D _h = Hole Diameter (in) |
|-------------------------|--|--|
| BF = | <u>65.50 - W</u> 65.50 | BF = Buoyancy Factor W = Mud Weight (Ib/gal) |
| BHIF = 0.1 | 0173 Q (P _b x W) ^{1/2} | BHIF = Bit Hydraulic Impact Force (Ib) Pb = Bit Pressure Drop (psi) W = Mud Weight (Ib/gal) |
| PS = - | PDS or - | PS = Pump Speed (stroke/min) Q = Flow Rate (gal/min) PDS = Pump Displacement (gal/ |
| PS = | AV x C PDS | AV = Annular Velocity (ft/sec) C = Annular Capacity |

MUD WEIGHT

| lb/gal | kg/l | lb/ft³ | kg/m ³ | Sp. Gr. | psi/ft | kPa/m |
|--------|------|--------|-------------------|---------|--------|-------|
| 8.3 | 0.99 | 62.08 | 994.43 | 1.00 | 0.431 | 9.75 |
| 8.4 | 1.01 | 62.83 | 1,006.44 | 1.01 | 0.436 | 9.86 |
| 8.5 | 1.02 | 63.58 | 1,018.45 | 1.02 | 0.441 | 9.98 |
| 8.6 | 1.03 | 64.33 | 1,030.47 | 1.04 | 0.447 | 10.11 |
| 8.7 | 1.04 | 65.08 | 1,042.48 | 1.05 | 0.452 | 10.22 |
| 8.8 | 1.05 | 65.82 | 1,054.34 | 1.06 | 0.457 | 10.34 |
| 8.9 | 1.07 | 66.57 | 1,066.35 | 1.07 | 0.462 | 10.45 |
| 9.0 | 1.08 | 67.32 | 1,078.36 | 1.08 | 0.467 | 10.56 |
| 9.1 | 1.09 | 68.07 | 1,090.38 | 1.10 | 0.472 | 10.68 |
| 9.2 | 1.10 | 68.82 | 1,102.39 | 1.11 | 0.478 | 10.81 |
| 9.3 | 1.11 | 69.56 | 1,114.24 | 1.12 | 0.483 | 10.93 |
| 9.4 | 1.13 | 70.31 | 1,126.26 | 1.13 | 0.488 | 11.04 |
| 9.5 | 1.14 | 71.06 | 1,138.27 | 1.14 | 0.493 | 11.15 |
| 9.6 | 1.15 | 71.81 | 1,150.29 | 1.16 | 0.498 | 11.27 |
| 9.7 | 1.16 | 72.56 | 1,162.30 | 1.17 | 0.504 | 11.40 |
| 9.8 | 1.17 | 73.30 | 1,174.15 | 1.18 | 0.509 | 11.51 |
| 9.9 | 1.19 | 74.05 | 1,186.17 | 1.19 | 0.514 | 11.63 |
| 10.0 | 1.20 | 74.80 | 1,198.18 | 1.20 | 0.519 | 11.74 |
| 10.1 | 1.21 | 75.55 | 1,210.19 | 1.22 | 0.524 | 11.85 |
| 10.2 | 1.22 | 76.30 | 1,222.21 | 1.23 | 0.530 | 11.99 |
| 10.3 | 1.23 | 77.04 | 1,234.06 | 1.24 | 0.535 | 12.10 |
| 10.4 | 1.25 | 77.79 | 1,246.08 | 1.25 | 0.540 | 12.22 |
| 10.5 | 1.26 | 78.54 | 1,258.09 | 1.27 | 0.545 | 12.33 |
| 10.6 | 1.27 | 79.29 | 1,270.10 | 1.28 | 0.550 | 12.44 |
| 10.7 | 1.28 | 80.04 | 1,282.12 | 1.29 | 0.556 | 12.58 |
| 10.8 | 1.29 | 80.78 | 1,293.97 | 1.30 | 0.561 | 12.69 |
| 10.9 | 1.31 | 81.53 | 1,305.99 | 1.31 | 0.566 | 12.80 |
| 11.0 | 1.32 | 82.28 | 1,318.00 | 1.33 | 0.571 | 12.92 |
| 11.1 | 1.33 | 83.03 | 1,330.01 | 1.34 | 0.577 | 13.05 |
| 11.2 | 1.34 | 83.78 | 1,342.03 | 1.35 | 0.582 | 13.17 |
| 11.3 | 1.35 | 84.52 | 1,353.88 | 1.36 | 0.587 | 13.28 |
| 11.4 | 1.37 | 85.27 | 1,365.89 | 1.37 | 0.592 | 13.39 |
| 11.5 | 1.38 | 86.02 | 1,377.91 | 1.39 | 0.597 | 13.50 |
| 11.6 | 1.39 | 86.77 | 1,389.92 | 1.40 | 0.602 | 13.62 |
| 11.7 | 1.40 | 87.52 | 1,401.94 | 1.41 | 0.607 | 13.73 |
| 11.8 | 1.41 | 88.26 | 1,413.79 | 1.42 | 0.613 | 13.87 |
| 11.9 | 1.43 | 89.01 | 1,425.80 | 1.43 | 0.618 | 13.98 |
| 12.0 | 1.44 | 89.76 | 1,437.82 | 1.45 | 0.623 | 14.09 |
| 12.1 | 1.45 | 90.51 | 1,449.83 | 1.46 | 0.628 | 14.21 |
| 12.2 | 1.46 | 91.26 | 1,461.84 | 1.47 | 0.633 | 14.32 |
| 12.3 | 1.47 | 92.00 | 1,473.70 | 1.48 | 0.639 | 14.45 |
| 12.4 | 1.49 | 92.75 | 1,485.71 | 1.49 | 0.644 | 14.57 |
| 12.5 | 1.50 | 93.50 | 1,497.73 | 1.51 | 0.649 | 14.68 |
| 12.6 | 1.51 | 94.25 | 1,509.74 | 1.52 | 0.654 | 14.79 |

NOZZLE SELECTION

For proper sizing of the rotor nozzle, refer to the Motor Specification section and obtain the recommended flow rate through the motor at the desired RPM and differential pressure. Subtract this flow rate from the total desired flow rate to obtain the required flow rate through the nozzle (q). Adjust this flow rate for the actual mud weight as follows:

 $Q = q \times 0.35 \times \sqrt{(Mud Weight)}$ (gal/min) (gal/min) (lb/gal)

Using Q and the desired motor differential pressure, determine the nozzle size from the graph below. Use the next smaller nozzle if between sizes.

Example

A $6\frac{34}{7}$, 4:5, 7.0 stage extended drilling motor is used to drill a well. A 12.5 lb/gal mud at 750 gal/min will be used to complete this well. If the motor is operated at 700 psi of differential pressure, determine if it is necessary to nozzle the rotor. If so, what is the proper nozzle size?

Solution

The maximum allowable flow rate through a $6\frac{3}{7}$, 4:5, 7.0 stage extended drilling motor is 600 gal/min, as listed in the Motor Specification section. Therefore, the additional 150 gal/min should bypass the power section through the rotor.

To determine the nozzle size, first adjust the flow rate for the actual mud weight:

Q = 150 x 0.35 x (12.5)^{0.5} = 185.62 gal/min

The nozzle selection graph shows that pumping 185.62 gal/min at 700 psi differential pressure requires a 16/32 nozzle.



DRILL COLLAR WEIGHT (LB/FT)

| 0.0 | Inside Diameter (in) | | | | | | | | | | | | |
|-------|----------------------|----|-----|-----|-----|------|-----|--------------------|-----|-----|-----|-----|-----|
| (in) | - | 1% | 1½ | 1¾ | 2 | 21⁄4 | 2½ | 2 ^{13/16} | ω | 3¼ | 3½ | 3¾ | 4 |
| 2 % | 19 | 18 | 16 | | | | | | | | | | |
| 3 | 21 | 20 | 18 | | | | | | | | | | |
| 31⁄8 | 22 | 22 | 20 | | | | | | | | | | |
| 3¼ | 26 | 24 | 22 | | | | | | | | | | |
| 3½ | 30 | 29 | 27 | | | | | | | | | | |
| 3¾ | 35 | 33 | 32 | | | | | | | | | | |
| 4 | 40 | 39 | 37 | 35 | 32 | 29 | | | | | | | |
| 4 1⁄8 | 43 | 41 | 39 | 37 | 35 | 32 | | | | | | | |
| 4 1⁄4 | 46 | 44 | 42 | 40 | 38 | 35 | | | | | | | |
| 4 1/2 | 51 | 50 | 48 | 46 | 43 | 41 | | | | | | | |
| 4 3⁄4 | | | 54 | 52 | 50 | 47 | 44 | | | | | | |
| 5 | | | 61 | 59 | 56 | 53 | 50 | | | | | | |
| 5 1/4 | | | 68 | 65 | 63 | 60 | 57 | | | | | | |
| 5½ | | | 75 | 73 | 70 | 67 | 64 | 60 | | | | | |
| 5 ¾ | | | 82 | 80 | 78 | 75 | 72 | 67 | 64 | 60 | | | |
| 6 | | | 90 | 88 | 85 | 83 | 79 | 75 | 68 | 68 | | | |
| 6 1⁄4 | | | 98 | 96 | 94 | 91 | 88 | 83 | 76 | 76 | 72 | | |
| 6½ | | | 107 | 105 | 102 | 99 | 96 | 91 | 85 | 85 | 80 | | |
| 6 ¾ | | | 116 | 114 | 111 | 108 | 105 | 100 | 93 | 93 | 89 | | |
| 7 | | | | | 120 | 117 | 114 | 110 | 103 | 103 | 98 | 93 | 94 |
| 7 1⁄4 | | | | | 130 | 127 | 124 | 119 | 112 | 112 | 108 | 103 | 93 |
| 7½ | | | | | 139 | 137 | 133 | 129 | 122 | 122 | 117 | 113 | 102 |
| 7 ¾ | | | | | 150 | 147 | 144 | 139 | 132 | 132 | 128 | 123 | 112 |
| 8 | | | | | 160 | 157 | 154 | 150 | 143 | 143 | 138 | 133 | 122 |
| 8 1⁄4 | | | | | 171 | 168 | 165 | 160 | 154 | 154 | 149 | 144 | 133 |
| 8½ | | | | | 182 | 179 | 176 | 172 | 165 | 165 | 160 | 155 | 150 |
| 9 | | | | | | 203 | 200 | 195 | 188 | 188 | 184 | 179 | 174 |
| 9½ | | | | | | 227 | 224 | 220 | 212 | 212 | 209 | 206 | 198 |
| 9 ¾ | | | | | | 240 | 237 | 232 | 225 | 225 | 221 | 216 | 211 |
| 10 | | | | | | 254 | 251 | 246 | 239 | 239 | 235 | 230 | 225 |
| 11 | | | | | | 310 | 307 | 302 | 295 | 295 | 291 | 286 | 281 |
| 12 | | | | | | 371 | 368 | 364 | 357 | 357 | 352 | 347 | 342 |

CASING DIMENSIONS AND BIT CLEARANCE

| OD (in) | Weight (lb/ft) | Wall | ID | Coupling OD | Drift | Bit Size | Clearance |
|------------|-------------------|-------|-------|----------------|-------|-------------------|-----------|
| 4 1/2 | 9.50 | 0.205 | 4.090 | 5.000 | 3.965 | 31%8 | 0.090 |
| | 11.60 | 0.205 | 4.000 | 5.000 | 3.875 | 31⁄8 | 0.000 |
| | 13.50 | 0.290 | 3.920 | 5.000 | 3.795 | 3¾ | 0.045 |
| | 15.10 | 0.337 | 3.826 | 5.000 | 3.701 | 35⁄8 | 0.078 |
| | | | | | | | |
| 5 | 11.50 | 0.220 | 4.560 | 5.563 | 4.435 | 4¼ | 0.185 |
| | 13.00 | 0.253 | 4.494 | 5.563 | 4.369 | 4¼ | 0.119 |
| | 15.00 | 0.296 | 4.408 | 5.563 | 4.283 | 4¼ | 0.033 |
| | 18.00 | 0.362 | 4.276 | 5.563 | 4.151 | 41⁄8 | 0.026 |
| | | | | | | | |
| 5½ | 13.00 | 0.228 | 5.044 | 6.050 | 4.919 | 4¾ | 0.169 |
| | 14.00 | 0.244 | 5.012 | 6.050 | 4.887 | 4¾ | 0.137 |
| | 15.50 | 0.275 | 4.950 | 6.050 | 4.825 | 4¾ | 0.075 |
| | 17.00 | 0.304 | 4.892 | 6.050 | 4.767 | 4¾ | 0.017 |
| | 20.00 | 0.361 | 4.778 | 6.050 | 4.653 | 4 5⁄8 | 0.028 |
| _ | 23.00 | 0.415 | 4.670 | 6.050 | 4.545 | 4½ | 0.045 |
| | | | | | | | |
| 6 | 15.00 | 0.238 | 5.524 | 6.625 | 5.399 | 5¾ | 0.024 |
| | 18.00 | 0.288 | 5.425 | 6.625 | 5.299 | 51⁄8 | 0.174 |
| | 20.00 | 0.324 | 5.352 | 6.625 | 5.227 | 51⁄8 | 0.102 |
| | 23.00 | 0.380 | 5.240 | 6.625 | 5.115 | 41⁄8 | 0.240 |
| | 26.00 | 0.434 | 5.132 | 6.625 | 5.007 | 41⁄8 | 0.132 |
| | | | | | | | |
| 6 5/8 | 17.00 | 0.245 | 6.135 | 7.390 | 6.010 | 6 | 0.010 |
| | 20.00 | 0.288 | 6.049 | 7.390 | 5.924 | 5% | 0.049 |
| | 24.00 | 0.352 | 5.921 | 7.390 | 5.769 | 5¾ | 0.046 |
| | 28.00 | 0.417 | 5.791 | 7.390 | 5.666 | 5 % | 0.014 |
| | 32.00 | 0.475 | 5.675 | 7.390 | 5.550 | 5¾ | 0.175 |
| | | | | | | | |
| 7 | 17.00 | 0.231 | 6.538 | 7.656 | 6.413 | 63⁄8 | 0.038 |
| | 20.00 | 0.272 | 6.456 | 7.656 | 6.331 | 6¼ | 0.081 |
| | 23.00 | 0.317 | 6.366 | 7.656 | 6.241 | 61⁄8 | 0.116 |
| | 26.00 | 0.362 | 6.276 | 7.656 | 6.151 | 61⁄8 | 0.026 |
| | 29.00 | 0.408 | 6.184 | 7.656 | 6.059 | 6 | 0.059 |
| | 32.00 | 0.453 | 6.094 | 7.656 | 5.969 | 51% | 0.940 |
| | 35.00 | 0.498 | 6.004 | 7.656 | 5.879 | 51% | 0.004 |
| | 38.00 | 0.540 | 5.920 | 7.656 | 5.795 | 5 ³ ⁄4 | 0.045 |

CASING DIMENSIONS AND BIT CLEARANCE

| OD (in) | Weight (lb/ft) | Wall (in) | ID (in) | Coupling OD (in) | Drift (in) | Bit Size (in) | Clearance (in) |
|------------|-------------------|--------------|------------|---------------------|---------------|------------------|-------------------|
| 133⁄8 | 48.00 | 0.330 | 12.715 | 14.375 | 12.559 | 12¼ | 0.309 |
| | 54.50 | 0.380 | 12.615 | 14.375 | 12.459 | 12¼ | 0.209 |
| | 61.00 | 0.430 | 12.515 | 14.375 | 12.359 | 12¼ | 0.109 |
| | 68.00 | 0.480 | 12.415 | 14.375 | 12.259 | 12¼ | 0.009 |
| | 72.00 | 0.514 | 12.374 | 14.375 | 12.191 | 10 | 2.191 |
| | | | | | | | |
| 16 | 55.00 | 0.312 | 15.375 | 17.000 | 15.188 | 15 | 0.188 |
| | 65.00 | 0.375 | 15.250 | 17.000 | 15.062 | 15 | 0.062 |
| | 75.00 | 0.438 | 15.125 | 17.000 | 14.938 | 14¾ | 0.188 |
| | 84.00 | 0.495 | 15.010 | 17.000 | 14.823 | 14¾ | 0.073 |
| | | | | | | | |
| 20 | 94.00 | 0.438 | 19.124 | 21.000 | 18.938 | 17½ | 1.436 |

RECOMMENDED MINIMUM MAKE-UP TORQUE

Protective Sleeve & Near Bit Stabilizer Make-up Torque Values

| Tool Size | Toro | ue |
|--------------------|--------|--------|
| 1001 3120 | ft-lbs | Nm |
| 3 ³⁄4" | 6,500 | 8,813 |
| 4³⁄4″ | 11,000 | 14,914 |
| 6¼" | 17,000 | 23,049 |
| 6 1⁄2" | 26,500 | 35,929 |
| 6 ¾″ | 26,500 | 35,929 |
| 7 ¼″ | N/A | N/A |
| 8" | 29,000 | 39,319 |
| 9 ⁵ ⁄8″ | 44,000 | 59,656 |

CASING DIMENSIONS AND BIT CLEARANCE

| OD (in) | Weight (lb/ft) | Wall (in) | ID (in) | Coupling OD (in) | Drift (in) | Bit Size (in) | Clearance (in) |
|------------|-------------------|--------------|------------|---------------------|---------------|------------------|-------------------|
| 7 5⁄8 | 20.00 | 0.250 | 7.125 | 8.500 | 7.000 | 6¾ | 0.250 |
| | 24.00 | 0.300 | 7.025 | 8.500 | 6.900 | 6¾ | 0.150 |
| | 26.40 | 0.328 | 6.969 | 8.500 | 6.844 | 6¾ | 0.094 |
| | 29.70 | 0.375 | 6.875 | 8.500 | 6.750 | 6¾ | 0.000 |
| | 33.70 | 0.430 | 6.765 | 8.500 | 6.640 | 65⁄8 | 0.015 |
| | 39.00 | 0.500 | 6.625 | 8.500 | 6.500 | 6¾ | 0.125 |
| | | | | | | | |
| 8 5/8 | 24.00 | 0.264 | 8.097 | 9.625 | 7.972 | 71⁄8 | 0.097 |
| | 28.00 | 0.304 | 8.017 | 9.625 | 7.892 | 71/8 | 0.017 |
| | 32.00 | 0.352 | 7.921 | 9.625 | 7.796 | 7¾ | 0.046 |
| | 36.00 | 0.400 | 7.825 | 9.625 | 7.700 | 75/8 | 0.075 |
| | 40.00 | 0.450 | 7.725 | 9.625 | 7.600 | 7¾ | 0.225 |
| | 44.00 | 0.500 | 7.625 | 9.625 | 7.500 | 73⁄8 | 0.125 |
| | 49.00 | 0.557 | 7.511 | 9.625 | 7.386 | 73⁄8 | 0.011 |
| | | | | | | | |
| 9 5⁄8 | 29.30 | 0.281 | 9.063 | 10.625 | 8.907 | 8¾ | 0.157 |
| | 32.30 | 0.312 | 9.001 | 10.625 | 8.845 | 8¾ | 0.095 |
| | 36.00 | 0.352 | 8.921 | 10.625 | 8.765 | 8¾ | 0.015 |
| | 40.00 | 0.395 | 8.835 | 10.625 | 8.697 | 85⁄8 | 0.072 |
| | 43.50 | 0.435 | 8.755 | 10.625 | 8.599 | 8½ | 0.099 |
| | 47.00 | 0.472 | 8.681 | 10.625 | 8.525 | 8½ | 0.025 |
| | 53.50 | 0.545 | 8.535 | 10.625 | 8.379 | 83⁄8 | 0.004 |
| | | | | | | | |
| 10¾ | 32.75 | 0.279 | 10.192 | 11.750 | 10.036 | 97⁄8 | 0.161 |
| | 40.50 | 0.350 | 10.050 | 11.750 | 9.894 | 91⁄8 | 0.019 |
| | 45.50 | 0.400 | 9.920 | 11.750 | 9.794 | 9¾ | 0.044 |
| | 51.00 | 0.450 | 9.850 | 11.750 | 9.694 | 95⁄8 | 0.069 |
| | 55.50 | 0.495 | 9.760 | 11.750 | 9.604 | 9 | 0.630 |
| | 60.70 | 0.545 | 9.660 | 11.750 | 9.504 | 9 | 0.504 |
| | 65.70 | 0.595 | 9.560 | 11.750 | 9.404 | 9 | 0.404 |
| | | | | | | | |
| 11¾ | 38.00 | 0.300 | 11.150 | 12.750 | 10.994 | 105⁄8 | 0.369 |
| | 42.00 | 0.333 | 11.084 | 12.750 | 10.928 | 105⁄8 | 0.303 |
| | 47.00 | 0.375 | 11.000 | 12.750 | 10.844 | 105⁄8 | 0.219 |
| | 54.00 | 0.435 | 10.880 | 12.750 | 10.724 | 105⁄8 | 0.099 |
| | 60.00 | 0.489 | 10.772 | 12.750 | 10.616 | 9% | 0.741 |
| | | | | | | | |

| | | RECOM | MENDI | ED MIN | MUM | MAKE- | UP TOF | ROUE (F | T-LBS | | | | |
|-----------------------------|-------|-------|-------|--------|--------|--------|----------------------|--------------|--------------------|---|-----|------|----|
| Connection Tuno | | | | | | | Bore of Drill | Collars (in) | | | | | |
| | | - | 114 | 1½ | 1¾ | 2 | 2¼ | 21/2 | 2 ^{13/16} | m | 314 | 31/2 | 3¾ |
| | e | 2,500 | 2,500 | 2,500 | | | | | | | | | |
| API N.C. 23 | 31/8 | 3,300 | 3,300 | 2,600 | | | | | | | | | |
| | 314 | 4,000 | 3,400 | 2,600 | | | | | | | | | |
| | ° | | 3,800 | 3,800 | 2,900 | | | | | | | | |
| 2 7/8" P.A.C. | 3 ½s | | 4,900 | 4,200 | 2,900 | | | | | | | | |
| | 31/4 | | 5,200 | 4,200 | 2,900 | | | | | | | | |
| 2 78" AM 0.H. | 3 7/8 | | | | | 4,450* | | | | | | | |
| 27%" AM. O.H. Light weight | 3% | | | | | 2,850* | | | | | | | |
| 2 7/8" PH-6 | 3 ½ | | | | | 3,500* | | | | | | | |
| 2 %" 533 HYDRIL | 3 ½8 | | | | | 2,200* | | | | | | | |
| 238" API I.F., API N.C. 26 | 3 ½2 | | 4,600 | 4,600 | 3,700 | | | | | | | | |
| 2 78" Slim Hole | 3¾ | | 5,500 | 4,700 | 3,700 | | | | | | | | |
| 2 ³ %" XHOLE | 3% | | 4,100 | 4,100 | 4,100 | | | | | | | | |
| 31/2" Dbl. Streamline | 3 7/s | | 5,300 | 5,300 | 5,300 | | | | | | | | |
| 2 ⁷ 8" Mod. Open | 4 1/8 | | 8,000 | 8,000 | 7,400 | | | | | | | | |
| | 4 1/2 | | | | 8,900 | 8,900 | 8,900 | 7,400 | | | | | |
| API N.C. 35 | 43/4 | | | | 12,100 | 10,800 | 9,200 | 7,400 | | | | | |
| | 5 | | | | 12,100 | 10,800 | 9,200 | 7,400 | | | | | |

Note: The torque values are based on the minimum material yield strength of 120 kpsi. ID of 2" = 2.2.

RECOMMENDED MINIMUM MAKE-UP TORQUE (FT-LBS)

| Constitution Time | | | | | | | Bore of Uril | Collars (In) | | | | | |
|-------------------------------|--------------|---|---------|-------|--------|--------|--------------|--------------|--------------------|---|----|------|----|
| | | - | 1% | 1½ | 1¾ | 2 | 2¼ | 2 \% | 2 ^{13/16} | m | 3% | 31/2 | 3¾ |
| | 3 7/8 | | 4,600 | 4,600 | 4,600 | 4,600 | | | | | | | |
| 2 %" API I.F. | 4 1/8 | | 7,300 | 7,300 | 7,300 | 6,800 | | | | | | | |
| AFIN.C. 31 31/2" Slim Hole | 4 1/4 | | 8,800 | 8,800 | 8,100 | 6,800 | | | | | | | |
| | 41/2 | | 1 0,000 | 9,300 | 8,100 | 6,800 | | | | | | | |
| | 4 1/4 | | | | 5,100 | 5,100 | 5,100 | 5,100 | | | | | |
| 3 ½" XHOLE | 41/2 | | | | 8,400 | 8,400 | 8,400 | 8,200 | | | | | |
| 4" Slim Hole | 4 3/4 | | | | 11,900 | 11,700 | 10,000 | 8,200 | | | | | |
| 3 ½" Mod. Open | ß | | | | 13,200 | 11,700 | 10,000 | 8,200 | | | | | |
| | 514 | | | | 13,200 | 11,700 | 10,000 | 8,200 | | | | | |
| | 4 3/4 | | | | 006'6 | 006'6 | 006'6 | 0'600 | 8,300 | | | | |
| 3%" API I.F. | 2 | | | | 13,800 | 13,800 | 12,800 | 10,900 | 8,300 | | | | |
| AFIN.C. 30 414" Slim Hole | 514 | | | | 16,000 | 14,600 | 12,800 | 10,900 | 8,300 | | | | |
| | 51/2 | | | | 16,000 | 14,600 | 12,800 | 10,900 | 8,300 | | | | |
| | 4 3/4 | | | | 8,700 | 8,700 | 8,700 | 8,700 | 8,700 | | | | |
| 00 H #716 | ß | | | | 12,700 | 12,700 | 12,700 | 12,700 | 10,400 | | | | |
| 06-11 2/ 6 | 514 | | | | 16,900 | 16,700 | 15,000 | 13,100 | 10,400 | | | | |
| | 51/2 | | | | 18,500 | 16,700 | 15,000 | 13,100 | 10,400 | | | | |

Note: The torque values are based on the minimum material yield strength of 120 kpsi

| Connection Type | OD (in) | | ł | ; | | • | Bore of Drill | Collars (in) | | (| į | į | ć |
|---------------------|---------|---|----|----|--------|--------|---------------|--------------|--------------------|---|----|----|---|
| | | - | 1% | 1½ | 1¾ | 2 | 2¼ | 21/2 | 2 ^{13/16} | ო | 3¼ | 3½ | |
| | 5 | | | | 10,800 | 10,800 | 10,800 | 10,800 | 10,800 | | | | |
| 4" Full Hole | 514 | | | | 15,100 | 15,100 | 15,100 | 14,800 | 12,100 | | | | |
| API N.C. 40 | 5 ½ | | | | 19,700 | 18,600 | 16,900 | 14,800 | 12,100 | | | | |
| 4 k" DhI Streamline | 5 3/4 | | | | 20,400 | 18,600 | 16,900 | 14,800 | 12,100 | | | | |
| | 9 | | | | 20,400 | 18,600 | 16,900 | 14,800 | 12,100 | | | | |
| | 514 | | | | | 12,500 | 12,500 | 12,500 | 12,500 | | | | |
| | 5 1/2 | | | | | 17,300 | 17,300 | 17,300 | 16,500 | | | | |
| 4" H-90 | 5 3/4 | | | | | 22,300 | 21,500 | 19,400 | 16,500 | | | | |
| | 9 | | | | | 23,500 | 21,500 | 19,400 | 16,500 | | | | |
| | 61/4 | | | | | 23,500 | 21,500 | 19,400 | 16,500 | | | | |
| | 5 ½ | | | | | 15,400 | 15,400 | 15,400 | 15,400 | | | | |
| | 5 3/4 | | | | | 20,300 | 20,300 | 19,400 | 16,200 | | | | |
| 4 /2 API Regular | 9 | | | | | 23,400 | 21,600 | 19,400 | 16,200 | | | | |
| | 6¼ | | | | | 23,400 | 21,600 | 19,400 | 16,200 | | | | |
| | 5 3/4 | | | | | 20,600 | 20,600 | 20,600 | 18,000 | | | | |
| ADI NI C. 44 | 9 | | | | | 25,000 | 23,300 | 21,200 | 18,000 | | | | |
| API N.C. 44 | 614 | | | | | 25,000 | 23,300 | 21,200 | 18,000 | | | | |
| | 6 ½ | | | | | 25,000 | 23,300 | 21,200 | 18,000 | | | | |

Note: The torque values are based on the minimum material yield strength of 120 kpsi

RECOMMENDED MINIMUM MAKE-UP TORQUE (FT-LBS)

| Connection Tuno | (ui) OO | | | | | | Bore of Drill | Collars (in) | | | | | |
|--------------------|---------|---|----|------|------|--------|---------------|--------------|---------------------|--------|----|----|----|
| | | - | 1% | 11/2 | 13/4 | 2 | 2¼ | 21/2 | 2 ¹³ /16 | m | 3¼ | 3½ | 3¾ |
| | 5 ½ | | | | | 12,900 | 12,900 | 12,900 | 12,900 | 12,900 | | | |
| | 5 3/4 | | | | | 17,900 | 17,900 | 17,900 | 17,900 | 17,700 | | | |
| 4 ½" API Full Hole | 9 | | | | | 23,300 | 23,300 | 22,800 | 19,800 | 17,700 | | | |
| | 6 14 | | | | | 27,000 | 25,000 | 22,800 | 19,800 | 17,700 | | | |
| | 6 ½ | | | | | 27,000 | 25,000 | 22,800 | 19,800 | 17,700 | | | |
| 4 ½" X-Hole | 5 3/4 | | | | | | 17,600 | 17,600 | 17,600 | 17,600 | | | |
| API N.C. 46 | 9 | | | | | | 23,200 | 23,200 | 22,200 | 20,200 | | | |
| 4 ½" Mod. Open | 6 14 | | | | | | 28,000 | 25,500 | 22,200 | 20,200 | | | |
| 4" API I.F. | 6 ½ | | | | | | 28,000 | 25,500 | 22,200 | 20,200 | | | |
| 5" Dbl. Streamline | 6 3/4 | | | | | | 28,000 | 25,500 | 22,200 | 20,200 | | | |
| | 5 3/4 | | | | | | 17,600 | 17,600 | 17,600 | 17,600 | | | |
| | 9 | | | | | | 23,400 | 23,400 | 23,000 | 21,000 | | | |
| 4 ½" H-90 | 6 1/4 | | | | | | 28,500 | 26,000 | 23,000 | 21,000 | | | |
| | 6 ½ | | | | | | 28,500 | 26,000 | 23,000 | 21,000 | | | |
| | 6 3/4 | | | | | | 28,500 | 26,000 | 23,000 | 21,000 | | | |
| | 6 1/4 | | | | | | 25,000 | 25,000 | 25,000 | 25,000 | | | |
| 5" H 00 | 6 ½ | | | | | | 31,500 | 31,500 | 29,500 | 27,000 | | | |
| 06-11 0 | 6 3/4 | | | | | | 35,000 | 33,000 | 29,500 | 27,000 | | | |
| | 7 | | | | | | 35,000 | 33,000 | 29,500 | 27,000 | | | |
| | | | | | | | | | | | | | |

Note: The torque values are based on the minimum material yield strength of 120 kpsi

RECOMMENDED MINIMUM MAKE-UP TORQUE (FT-LBS)

| F | | | | | | | Bore of Drill | Collars (in) | | | | | |
|----------------------|-------|---|------|----|------|---|---------------|--------------|--------------------|--------|--------|----|----|
| | | - | 11/4 | 1½ | 13/4 | 2 | 2¼ | 21/2 | 2 ^{13/16} | m | 3¼ | 3½ | 3¾ |
| | 6 3/4 | | | | | | 34,000 | 34,000 | 34,000 | 34,000 | | | |
| 517" L 00 | 7 | | | | | | 41,500 | 40,000 | 36,500 | 34,000 | | | |
| 06-11 20 6 | 71/4 | | | | | | 42,500 | 40,000 | 36,500 | 34,000 | | | |
| | 71/2 | | | | | | 42,500 | 40,000 | 36,500 | 34,000 | | | |
| | 6 3/4 | | | | | | 31,500 | 31,500 | 31,500 | 31,500 | | | |
| | 7 | | | | | | 39,000 | 39,000 | 36,000 | 33,500 | | | |
| o 22 AFI hegular | 71/4 | | | | | | 42,000 | 39,500 | 36,000 | 33,500 | | | |
| | 71/2 | | | | | | 42,000 | 39,500 | 36,000 | 33,500 | | | |
| 4 ½" API I.F. | 61/4 | | | | | | 22,800 | 22,800 | 22,800 | 22,800 | 22,800 | | |
| API N.C. 50 | 61/2 | | | | | | 29,500 | 29,500 | 29,500 | 29,500 | 26,500 | | |
| 5" Extra Hole | 6 3/4 | | | | | | 36,000 | 35,500 | 32,000 | 30,000 | 26,500 | | |
| 5" Mod. Open | 7 | | | | | | 38,000 | 35,500 | 32,000 | 30,000 | 26,500 | | |
| 5 ½" Dbl. Streamline | 7 1/4 | | | | | | 38,000 | 35,500 | 32,000 | 30,000 | 26,500 | | |
| | 7 | | | | | | | 32,500 | 32,500 | 32,500 | 32,500 | | |
| E14" ADI Evill Holo | 71/4 | | | | | | | 40,500 | 40,500 | 40,500 | 40,500 | | |
| | 71/2 | | | | | | | 49,000 | 47,000 | 45,000 | 41,500 | | |
| | 7 3/4 | | | | | | | 51,000 | 47,000 | 45,000 | 41,500 | | |

Note: The torque values are based on the minimum material yield strength of 120 kpsi

| | Æ | RECOM | MENDE | ED MIN | IMUM | MAKE- | UP TOF | RQUE (F | T-LBS) | | | | |
|------------------|----------------------|-------|-------|--------|------|-------|---------------|--------------|--------------------|--------|--------|----|----|
| F | ,) 00 | | | | | | Bore of Drill | Collars (in) | | | | | |
| connection type | | - | 11/4 | 1½ | 1¾ | 2 | 2¼ | 21/2 | 2 ^{13/16} | m | 314 | 3½ | 3¾ |
| | 71/4 | | | | | | | 40,000 | 40,000 | 40,000 | 40,000 | | |
| ADI N C E6 | 7 1/2 | | | | | | | 48,500 | 48,000 | 45,000 | 42,000 | | |
| API N.C. 30 | J 3⁄4 | | | | | | | 51,000 | 48,000 | 45,000 | 42,000 | | |
| | 8 | | | | | | | 51,000 | 48,000 | 45,000 | 42,000 | | |
| | 7 1/2 | | | | | | | 46,000 | 46,000 | 46,000 | 46,000 | | |
| | 7 3⁄4 | | | | | | | 55,000 | 53,000 | 50,000 | 47,000 | | |
| 0.78 AFI hegular | 8 | | | | | | | 57,000 | 53,000 | 50,000 | 47,000 | | |
| | 81/4 | | | | | | | 57,000 | 53,000 | 50,000 | 47,000 | | |
| | 7 ½ | | | | | | | 46,000 | 46,000 | 46,000 | 46,000 | | |
| 227 " H-00 | ₽% L | | | | | | | 55,000 | 55,000 | 53,000 | 49,500 | | |
| 0.6-11 8/0 | 8 | | | | | | | 59,500 | 56,000 | 53,000 | 49,500 | | |
| | 81/4 | | | | | | | 59,500 | 56,000 | 53,000 | 49,500 | | |
| | 80 | | | | | | | 54,000 | 54,000 | 54,000 | 54,000 | | |
| | 81/4 | | | | | | | 64,000 | 64,000 | 64,000 | 61,000 | | |
| API N.C. 61 | 8 ½2 | | | | | | | 72,000 | 68,000 | 65,000 | 61,000 | | |
| | 8 ¾ | | | | | | | 72,000 | 68,000 | 65,000 | 61,000 | | |
| | 6 | | | | | | | 72,000 | 68,000 | 65,000 | 61,000 | | |

Note: The torque values are based on the minimum material yield strength of 120 kpsi

RECOMMENDED MINIMUM MAKE-UP TORQUE (FT-LBS)
| E | | | | | | | Bore of Drill | Collars (in) | | | | | |
|--------------------|--------|---|------|----|------|---|---------------|--------------|--------------------|----------|---------|--------|--------|
| | | - | 11/4 | 1½ | 13/4 | 2 | 2¼ | 21/2 | 2 ^{13/16} | m | 3¼ | 3½ | 3¾ |
| | 8 | | | | | | | 56,000 | 56,000 | 56,000 | 56,000 | 56,000 | |
| | 8 1/4 | | | | | | | 66,000 | 66,000 | 66,000 | 63,000 | 59,000 | |
| | 81/2 | | | | | | | 74,000 | 70,000 | 67,000 | 63,000 | 59,000 | |
| 372 APTI.F. | 8 3/4 | | | | | | | 74,000 | 70,000 | 67,000 | 63,000 | 59,000 | |
| | 6 | | | | | | | 74,000 | 70,000 | 67,000 | 63,000 | 59,000 | |
| | 9 1⁄4 | | | | | | | 74,000 | 70,000 | 67,000 | 63,000 | 59,000 | |
| | 81/2 | | | | | | | | 67,000 | 67,000 | 67,000 | 67,000 | 66,500 |
| | 8 3/4 | | | | | | | | 78,000 | 78,000 | 76,000 | 72,000 | 66,500 |
| 65%" API Full Hole | 6 | | | | | | | | 83,000 | 80,000 | 76,000 | 72,000 | 66,500 |
| | 91/4 | | | | | | | | 83,000 | 80,000 | 76,000 | 72,000 | 66,500 |
| | 9½ | | | | | | | | 83,000 | 80,000 | 76,000 | 72,000 | 66,500 |
| | 6 | | | | | | | | 75,000 | 75,000 | 75,000 | 75,000 | 75,000 |
| | 91/4 | | | | | | | | 88,000 | 88,000 | 88,000 | 88,000 | 88,000 |
| ADIN C 70 | 9½ | | | | | | | | 101,000 | 101,000 | 100,000 | 95,000 | 000'06 |
| ALIN.C. 10 | 9% | | | | | | | | 107,000 | 105,000 | 100,000 | 95,000 | 000'06 |
| | 10 | | | | | | | | 107,000 | 1 05,000 | 100,000 | 95,000 | 000'06 |
| | 10 1/4 | | | | | | | | 107,000 | 105,000 | 100,000 | 95,000 | 000'06 |

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| Pomootion Tumo | | | | | | | Bore of Drill | Collars (in) | | | | | |
|-----------------|--------|---|----|----|----|---|----------------------|--------------|--------------------|---------|---------|---------|---------|
| connection Lype | | - | 1% | 1½ | 1¾ | 2 | 2¼ | 21/2 | 2 ^{13/16} | m | 314 | 31/2 | 3¾ |
| | 10 | | | | | | | | | 107,000 | 107,000 | 107,000 | 107,000 |
| | 1014 | | | | | | | | | 122,000 | 122,000 | 122,000 | 122,000 |
| API N.C. 77 | 10 ½ | | | | | | | | | 138,000 | 138,000 | 133,000 | 128,000 |
| | 10 3/4 | | | | | | | | | 143,000 | 138,000 | 133,000 | 128,000 |
| | F | | | | | | | | | 143,000 | 138,000 | 133,000 | 128,000 |
| | 80 | | | | | | | | 53,000 | 53,000 | 53,000 | 53,000 | |
| 7" H-90 | 8 1/4 | | | | | | | | 63,000 | 63,000 | 63,000 | 60,500 | |
| | 8½ | | | | | | | | 71,500 | 68,500 | 65,000 | 60,500 | |

RECOMMENDED MINIMUM MAKE-UP TORQUE (FT-LBS)

Note: The torque values are based on the minimum material yield strength of 120 kpsi

8½ 8¾ 9¼ 9½

75%" API Regular

60,000 71,000 74,000 74,000 74,000

60,000 71,000 79,000 79,000

60,000 71,000 83,000 83,000

60,000 71,000 83,000 88,000 88,000

RECOMMENDED MINIMUM MAKE-UP TORQUE (FT-LBS)

| | | RECOM | MEND | ED MIN | NUW | 1 MAKI | E-UP TC | RQUE (| FT-LBS | () | | | |
|--------------------|--------|-------|------|--------|-----|--------|-----------|------------------|--------------------|---------|---------|---------|---------|
| Contraction T.m. | | | | | | | Bore of D | rill Collars (ii | Ē | | | | |
| | | - | 1% | 11% | 134 | 2 | 2¼ | 21/2 | 2 ^{13/16} | m | 3¼ | 3½ | 3¾ |
| | 6 | | | | | | | | | 72,000 | 72,000 | 72,000 | 72,000 |
| 7 5⁄6" H -90 | 91/4 | | | | | | | | | 85,500 | 85,500 | 85,500 | 85,500 |
| | 9 1/2 | | | | | | | | | 98,000 | 98,000 | 98,000 | 95,500 |
| | 10 | | | | | | | | | 108,000 | 108,000 | 108,000 | 108,000 |
| 8 5/8" API Regular | 10 1/4 | | | | | | | | | 123,000 | 123,000 | 123,000 | 123,000 |
| | 10 1/2 | | | | | | | | | 139,000 | 134,000 | 129,000 | 123,000 |
| 00/11 00 | 10 1/4 | | | | | | | | | 112,500 | 112,500 | 112,500 | 112,500 |
| 06-LI 8/0 | 10 1/2 | | | | | | | | | 128,500 | 128,500 | 128,500 | 128,500 |
| | | | | | | | | | | | | | |

Note: The torque values are based on the minimum material yield strength of 120 kpsi

ROTARY SHOULDER CONNECTION INTERCHANGE LIST

| Common Name | Size (in) | Same As or Interchanges With |
|------------------------------|--------------|---|
| Internal | 2 3⁄8 | 2% in Slim Hole NC 26 |
| Flush (IF) | 2 % | 31/2 in Slim Hole NC 31 |
| | 3½ | 41/2 in Slim Hole NC 38 |
| | 4 | 41/2 in Extra Hole NC 46 |
| | 4½ | 5 in Extra Hole NC 50 or 5½ in Double Streamline |
| Full Hole (FH) | 4 | 4½ in Double Streamline NC 40 |
| Extra Hole (XH) | 2 % | 3½ in Double Streamline |
| or (EH) | 3½ | 4 in Slim Hole or 4½ in External Flush |
| | 4½ | 4 in Internal Flush NC 46 |
| | 5 | 4½ in Internal Flush NC 50 or 5½ in Double Streamline |
| Slim Hole (SH) | 2 1/8 | 2% in Internal Flush NC 26 |
| | 3½ | 2% in Internal Flush NC 31 |
| | 4 | 3½ in Extra Hole or 4½ in External Flush |
| | 41⁄2 | 31/2 in Internal Flush NC 38 |
| Double Streamline | 3½ | 2% in Extra Hole |
| (DSL) | 4 1/2 | 4 in. Full Hole NC 31 |
| | 5½ | 4½ in Internal Flush or 5 in Extra Hole NC 50 |
| Numbered Connections (NC) | 26 | 2% in Internal flush or 2% in Slim Hole |
| | 31 | 2 % in Internal Flush or 3 ½ in Slim Hole |
| | 38 | 3½ in Internal Flush or 4½ in Slim Hole |
| | 40 | 4 in Full Hole or 4½ in Double Streamline |
| | 46 | 4 in Internal Flush or 4½ in Extra Hole |
| | 50 | 4½ in Internal Flush or 5 in Extra Hole or 5½ in Double Streamline |
| External Flush (EF) | 4½ | 4 in Slim Hole or 3½ in Extra Hole |

HEAVY-WALL DRILL PIPE PROPERTIES

Standard

| Nominal Size (in) | Pipe ID (in) | Nominal Weight (lb/ft) | Tool Joint Connection (in) |
|-------------------------|--------------------|------------------------------|----------------------------------|
| 3½" | 2.063 | 25.3 | 3.5 IF (NC 38) |
| 4" | 2.563 | 29.7 | 4 FH (NC 40) |
| 4½" | 2.75 | 41.0 | 4 IF (NC 46) |
| 5″ | 3.0 | 48.5 | 4.5 IF (NC 50) |

TORSIONAL ANGLE OF DRILL PIPE

The effective angle of torsion is calculated by:

 $\begin{array}{rcl} \text{Torsional} \\ \text{Angle} \end{array} = & \begin{array}{r} (\text{Angle for 1,000 ft}) \times (\text{Length of } D_{P}/\text{ft}) \\ 1,000 \end{array}$

**Calculation does not include wall friction



Spiral-Wate™

| Nominal Size (in) | Pipe ID (in) | Nominal Weight (lb/ft) | Tool Joint Connection (in) |
|-------------------------|--------------------|------------------------------|----------------------------------|
| 3½" | 2.25 | 26.7 | 3.5 IF (NC 38) |
| 4" | 2.563 | 32.7 | 4 FH (NC 40) |
| 41⁄2" | 2.75 | 42.6 | 4 IF (NC 46) |
| 5" | 3.0 | 53.6 | 4.5 IF (NC 50) |
| 5½" | 4.0 | 50.7 | 5 FH |
| 6 %" | 5.0 | 57.0 | 6.625 FH |

CONVERSION FACTORS

SI Prefixes

| Multiplying Factor | Prefix | Symbol |
|------------------------------|--------|--------|
| 1,000,000 = 10 ⁶ | mega | М |
| 1,000 = 10 ³ | kilo | k |
| 100 = 10 ² | hecto | h |
| 10 = 10 ¹ | deca | da |
| 0.1 = 10 ⁻¹ | deci | d |
| 0.01 = 10 ⁻² | centi | с |
| 0.001 = 10 ⁻³ | milli | m |
| 0.000,001 = 10 ⁻⁶ | micro | μ |

| Units | Multiply By | To Obtain |
|--------------------|----------------------------|--------------------|
| ac | 43560 | ft² |
| ac | 4047 | m² |
| ac | 0.001562 | mi² |
| atm | 33.94 | ft of water (60°F) |
| atm | 14.7 | lb/in ² |
| atm | 1.013 x 10⁵ | pascals |
| atm | 1.033 | kg/cm ² |
| bbl (British, dry) | 5.78 | ft³ |
| bbl (British, dry) | 0.1637 | m ³ |
| bbl (British, dry) | 36 | gal (British) |
| bbl, cement | 170.6 | kg |
| bbl, cement | 376 | lb (cement) |
| bbl, oil | 42 | gal (U.S.) |
| bbl (U.S., liquid) | 4.211 | ft³ |
| bbl (U.S., liquid) | 0.1192 | m³ |
| bbl (U.S., liquid) | 31.5 | gal (U.S.) |
| bbl/min | 42 | gal/min |
| bbl/day | 0.02917 | gal/min |
| cm | 0.3937 | in |
| cm | 3.281 x 10 ⁻² | ft |
| cm ³ | 3.531 x 10 ⁻⁵ | ft ³ |
| deg (angle) | 60 | min |
| deg (angle) | 0.01745 | rad |
| deg (angle) | 3600 | s |
| deg/s | 0.1667 | rpm |
| deg/s | 2.778 x 10 ⁻³ | rev/s |
| ft | 12 | in |
| ft | 0.3048 | m |
| ft | 1.89394 x 10 ⁻⁴ | mi |

| Units | Multiply By | To Obtain |
|---------------------------------|---------------------------|--------------------|
| ft² | 0.0929 | m² |
| ft³ | 1728 | in³ |
| ft ³ | 0.02832 | m ³ |
| ft ³ | 7.481 | gal (U.S.) |
| ft ³ | 28.32 | liters |
| ft ³ of water (60°F) | 62.37 | lb |
| ft³/min | 4.72 x 10 ⁻⁴ | m³/s |
| ft³/min | 0.1247 | gal/s |
| ft³/min | 0.472 | liters/s |
| ft³/s | 448.83 | gal/min |
| ft ³ - atm | 2116.3 | ft-lb |
| ft-lb | 1.286 x 10 ⁻³ | Btu |
| ft-lb | 0.1383 | kg/m |
| ft-lb | 1.355818 | Nm |
| ft/min | 0.508 | cm/s |
| ft/min | 0.01667 | ft/s |
| ft/min | 0.01829 | km/hr |
| ft/min | 0.3048 | m/min |
| ft/min | 0.01136 | mi/hr |
| ft-lb/min | 0.01667 | ft-lb/s |
| ft-lb/min | 2.26 x 10 ⁻⁵ | kW |
| ft-lb/s | 1.356 x 10 ⁻³ | kW |
| ft-lb/s | 1.818 x 10 ⁻³ | hp |
| g | 0.001 | kg |
| gal (British) | 1.20094 | gal (U.S.) |
| gal | 3785 | cm ³ |
| gal | 0.1337 | ft ³ |
| gal | 231 | in³ |
| gal | 3.785 | liters |
| gal/min | 2.228 x 10 ⁻³ | ft³/s |
| gal/min | 3.785 | liters/min |
| g-cm ² | 3.4172 x 10 ⁻⁴ | lb-in ² |
| hp | 0.7457 | kW |
| in | 25.4 | mm |
| in ² | 645.2 | mm ² |
| in ² | 6.452 | cm ² |
| in² | 6.944 x 10 ⁻³ | ft² |
| in³ | 1.639 x 10 ⁻⁵ | m ³ |
| in³ | 5.787 x 10 ⁻⁴ | ft ³ |
| in ³ | 4.329 x 10 ⁻³ | gal |
| in³ | 0.01639 | liters |
| in³ | 1000 | liters |

| Units | Multiply By | To Obtain |
|--------------------|--------------------------|--------------------|
| kg | 2.2046 | lb |
| kg-m | 7.233 | ft-lb |
| kg/m³ | 0.06243 | lb/ft ³ |
| kg/m | 0.672 | lb/ft |
| kW | 4.462 x 104 | ft-lb/min |
| kW-hr | 2.655 x 10 ⁶ | ft-lb |
| lb | 4.45 x 10⁵ | dynes |
| lb | 4.448 | newtons |
| lb | 4.535 x 10 ⁻⁴ | tons (metric) |
| lb/ft ³ | 16.02 | kg/m³ |
| lb/ft ³ | 5.787 x 10 ⁻⁴ | lb/in ³ |
| lb/ft ² | 4.882 | kg/m² |
| lb/ft ² | 6.945 x 10 ⁻³ | lb/in ² |
| lb/gal | 7.48 | lb/ft ³ |
| lb/gal | 0.12 | specific gravity |
| lb/gal | 0.1198 | g/cm ³ |
| lb/in ² | 6.894757 | kPa |
| liter | 0.03531 | ft ³ |
| liter | 0.001 | m³ |
| liter | 0.2642 | gal |
| m | 3.2808 | ft |
| m² | 10.764 | ft² |
| m ³ | 264.2 | gal |
| m³/s | 15850 | gal/min |
| m³/s | 60000 | liters/min |
| mi² | 2.788 x 10 ⁷ | ft² |
| mi² | 2.59 | km² |
| rad | 57.3 | deg |
| rad/s | 0.1592 | rev/s |
| rad/s | 9.549 | rpm |
| tons (metric) | 1000 | kg |
| W | 0.7376 | ft-lb/s |
| W | 1.341 x 10 ⁻³ | hp |
| yds | 3 | ft |
| yds | 0.9144 | m |

| Temperature | Conversion |
|---------------------------------|-------------------|
| Fahrenheit (°F) to Celsius (°C) | (5/9) x (°F - 32) |
| Celsius (°C) to Fahrenheit (°F) | 1.8 x °C + 32 |

BIT OFF-BOTTOM TROUBLESHOOTING CHART

| Primary Indication | Possible Cause | Subsequent Mode of Action |
|--|----------------------|---|
| Drop in circulating pressure to lower than calculated | Lost circulation | Lost circulation procedure |
| | Drill string washout | Pull out for check |
| | Open dump valve | Stop pumps, restart with increased flow, pull string if not corrected |
| Circulating pressure higher than calculated | Plugged motor or bit | Stop pumps, restart and vary flow rate, then reciprocate string |
| | Bit side-loading | Drill ahead carefully to relax tool assembly |

| Primary Indication | Secondary Indication | Possible Cause | Subsequent Mode of Action |
|---|--|---|---|
| No penetration | Drill Pipe Pressure (DPP) higher than maximum | Motor stall | Pull off-bottom to restart motor and apply WOB carefully |
| DPP rises higher than maximum calculated | No penetration | Motor stall | Pull off-bottom to restart motor and apply WOB carefully |
| | DPP rises – WOB normal | Broken or worn cutters. Bit "ringing" | Calculate cost-per-foot and either continue or pull out |
| | DPP falls – WOB normal | Hard formation or stabilizers hanging up | Continue with caution but if unsatisfactory, pull the bit |
| ROP decreases | DPP rises – Fails to respond to increased WOB | Bit balling | Lift off-bottom, reciprocate, then wash away balling material |
| | Slow fall in DPP | Bit is wearing | Calculate cost-per-foot and either continue or pull out |
| | DPP fluctuates | Assembly bouncing junk in hole | Attempt to wash away junk, then fish if unsuccessful |
| | DPP rises – WOB normal | Coffee formation and a state | Pull off-bottom, reassess angular reactive torque, then |
| Sudden rise in KOP | Tool Face Heading (TFH) turns to left | | continue drilling using recalculated parameters |

| ROP | SPP | WOB | Rotary Torque | Possible Cause | Subsequent Mode of Action |
|--------|------------|--------|------------------|---------------------------------|--|
| | | | Normal | Open dump valve or wash out | Stop pumps, restart, vary flow rate, then pull string if not corrected |
| | Falls | Normal | Rises | Stabilizers reaming | Continue with caution but if unsatisfactory, pull bit |
| | | | Falls | Harder formation encountered | Optimize ROP, then continue drilling |
| Falls | | | - H- L | Bit balling | Lift off-bottom, then reciprocate, wash away balling material |
| | Rises | Normal | Lalls | Bit ringing | Calculate cost-per-foot and either continue or pull bit |
| | | | Rises | Motor stall | Immediately stop rotary, then pull off-bottom and restart cautiously |
| | Fluctuates | Normal | Fluctuates | Junk in hole, bit cones locking | Attempt to wash away junk, then fish if necessary |
| - | Falls | Normal | Normal | Drill string wash-out | Pull out for check |
| Normal | Rises | Normal | Normal | Plugged motor or bit | Stop pump, restart and vary pressure, reciprocate string |
| Rises | Rises | Normal | Rises | Softer formation encountered | Optimize ROP, then continue drilling |

DRILLING WITH MOTOR ONLY TROUBLESHOOTING CHART

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DRILLING WITH MOTOR AND ROTARY TROUBLESHOOTING CHART

SCIENTIFIC SOLUTIONS

DIRECTIONAL DRILLING ROTARY STEERABLE SYSTEMS DRILLING MOTORS MAGNETIC RANGING CASED HOLE SERVICES MWD/LWD SERVICES WELLBORE SURVEYING DIGITAL SOLUTIONS

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